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Water Research Commission

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DOMESTIC WATER METERS: INFLUENCE OF VARIOUS FITTINGS AND INSTALLATION CONFIGURATIONS ON ACCURACY OF 15 MM WATER METERS

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Executive summary

The investigation into the effects of various fittings and installation configurations has become a necessity in view of the strict water loss controls brought by the promulgation of the new Water Services Act, 1997 (Act 108 of 1997), and the pending draft National Water Supply Regulations. Many of the water services authorities will base their work on reducing unaccounted-for water on SABS 0306:1999, a standard on the management of potable water in distribution systems. In coming up with a water audit report using the above mentioned code of practice, the water services authorities will have to use readings recorded from meters installed as the main part of their data, hence the need to correctly install the meters in order to get accurate readings. The current situation is that the installation of meters is being done by plumbers who are in some cases oblivious of the effect of haphazard installations and choice of fittings adjacent to the meter. As these meters are used for both domestic and industrial billing of consumers, the overregistration or underregistration due to their incorrect installation can result in false billing of consumers with resultant audit imbalances between the quantities of water actually supplied against water consumed. Water loss management as prescribed in the new draft National Water Supply Regulations can only be as accurate as the instruments used to measure the volumes of water. Unaccounted-for water brought, by unacceptable errors in meter indications have to be eliminated if the objectives of preserving water are to be achieved. The unit cost of purified water is going to become expensive owing to escalating purification, storing and transportation costs as well as scarcity owing to erratic weather patterns in the southern hemisphere, and therefore every drop of water needs to be accounted for.

Thus, the objectives of this research were to investigate the effects of various fittings and installation practices being currently employed in practice and come up with recommendations on the correct choice of fittings to be used adjacent to water meters as well as guidelines on correct installation. The objectives of this project were attained by subjecting two main types of 15mm diameter domestic meters, namely volumetric and inferential meters, to some of the conditions in which they are installed in practice and comparing the characteristics with standard meter performance characteristics. Tests were carried out in accordance with ISO 4064-3;1983 and SABS 1529-1:1994 standards on water meters. The meters were installed in a test bench in compatible groups, for example, inferential meters only. Readings were taken for the chosen flow rates and then compared with the actual volume of water through the meters as measured by a calibrated tank downstream of the meters. A constant head tank on the roof of the building ensured a steady flow of water through the meters. The percentage errors between the reading of the meter and the actual volume were then plotted against the corresponding flow rates and the resultant curves analysed.

By repeating the signature test twice, firstly at the beginning of the tests and again at the end, it was possible to determine whether the deviations in error versus flow-rate graphs were due to installation configurations being tested and not due to deterioration of the meter through wear and tear or change in environmental conditions. The first test involved inserting a 15mm ball valve at the inlet side of the meters and adjusting it so that it was fully open, 22,5° open and 45° open respectively. The second test involved rotating the meters 45° from the vertical and the third test had the meters installed with approved fittings (JASWIC; "R" Specifications, 1994) to simulate the above ground installation but without the inlet valve.

The following results emanated from the research:

- The 15rnm ball valve in various positions of opening at the inlet of the meters as well as the above ground installation did not produce any consistent notable effect on the meter accuracies
- The accuracy of certain models of volumetric meters was affected by the 45° tilt configuration,
 and
- The accuracy of the inferential, multi-jet type meters was affected in the lower flow rates below
 qt. (transitional flowrate) when the meters were rotated 45° from the vertical.

This research also indicated that more tests on all existing installation practices have to be carried out on all sizes of both single-jet and multi-jet inferential meters in order to be able to make comprehensive conclusions. The unusual phenomena exhibited by some volumetric meters requires further investigation.

Based on the results and interpretation thereof, the following recommendations are made:

- An inferential meter designed to operate in the horizontal standard position should always be
 installed with its turbine shaft axis coaxial with the vertical axis. More so there is need to
 investigate the critical angles or angular tolerance to which different models of meters start
 to lose sensitivity.
- The above ground installation does not impart large inaccuracies on meter performances and its use in meter installations where ease of reading is required, can still remain a normal practice.
- That an inlet ball valve of the type used in this research does not impart large inaccuracies on domestic meter performances. Emphasis is put on the words "type used in this research" as different valves impart different flow disturbance characteristics and therefore more types of valves should be tested.
- Better training curricula should be formulated for all plumbers to avoid improper installation
 of meters and increase their understanding of the importance of the information derived from
 a water meter in local government water management systems.
- Regular checks on meter manufacturers should be continued long after type approval to

ensure that they still produce their meters with accuracy and durability as key requirements.

This recommendation emanates from the fact that some type approved meters used in the research, failed the initial selection criteria.

 All municipalities and water governing bodies, plumbers institutions and other interested organizations should make use of the "Guidelines on Domestic Meter Installation Practices" which emanated from this study.

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GLOSSARY

Definitions

Accuracy: The comparison of the actual meter reading to the true value.

Water meter: Self contained integrating measuring instrument that continuously determine the volume of water flowing through them.

Potable water: Water that complies with the requirements of SABS 241.

Minimum flowrate(q_{min}): The lowest flowrate at which the meter is required to give indications within the permissible tolerance.

Overload flowrate(q_s):The flowrate that is equal to 2q_p and that represents the highest flowrate at which the meter is required to operate in a satisfactory manner for a short period of time without deterioration.

Permanent flowrate(q_P):The flowrate for which the meter is designed and at which the meter is required to give indications within the permissible tolerance under normal conditions of use.

Transitional flowrate(q_t): A flowrate that occurs between the permanent flowrate and the minimum flowrate and at which the flow is divided into two zones, the upper zone and the lower zone, each characterised by a specific permissible tolerance.

Abbreviations

BS: British Standard

CSIR: Centre for Scientific and Industrial Research

GMS: Galvanised mild steel

ISO: International Organisation for Standardisation

JASWIC: Joint Acceptance Scheme for Water Installation Components

NB: Nominal bore

OIML: International Organisation for Legal Metrology

SABS: South African Bureau of Standards

KEY TO GRAPH LEGENDS

ag: Above ground configuration

above ground ave.: Above ground configuration average curve

BV manifold 45 open ave: Ball valve configuration average curve with the valve 45 degree open.

T1, T2, T3 : Accuracy curves produced by plotting the percentage errors of the three meter readings taken at the same test flowrate.

Test manifold ave.: The average of the curves T1, T2, and T3

45 deg. tilt ave.: 45 degree configuration average curve

Background

This research to establish the influence of various fittings and installation configurations on the accuracy of a meter was initiated by the South African Bureau of Standards with financial assistance from the Water Research Commission. The pending new Water Regulations will prescribe water auditing as a requirement and the code of practice for "The management of potable water in distribution systems" (SABS 0306, 1999) will require accurate measurement of water passing through a water meter installation. It is therefore essential to measure and know the effect and contribution of meter accessories, fittings and pipe configurations used in installing a meter on the meter accuracy and performance. This will help to better inform and advise municipalities and contractors on the importance of correct choice of fittings and installation procedures. Haphazard meter installations and poor choice of materials having become the norm owing to deteriorating plumbing practices, the study of their impact on the meter accuracy is hence necessary. The relevance is that this understanding will contribute towards reducing the ensuing problems such as incorrect consumer billing, water loss audit imbalances and increase in unaccounted-for water thus rendering the water management systems by water authorities ineffective. A few examples of some existing poor installations are shown on photographs in Annex A.

This research first had to establish a reference or control as the basis for comparing the results of all the tests. Thus all the meters were initially tested in accordance with the requirements of South African Bureau of Standards (SABS1529-1,1994), which is similar to International Standard (ISO4064, 1983) regarding most aspects. To be able to see the performance of the meter over its entire range, twenty two flow rates instead of only five were tested and results were plotted against the percentage error in the volume reading shown by the meter to the actual volume as measured by a calibrated tank. Although the purpose of this research was not to verify the accuracies of the meters in ordinary calibration rigs, it is worth mentioning that some of the initial efficiency results did not comply with South African Bureau of Standards (SABS1529-1,1994) tolerances of 5% for flowrates less than the

transitional flowrate q_t and 2% for flowrates greater than q_t . This research focused more on the repeatability of the meter accuracy in various installation conditions.

The various configurations were then tested and the graphs obtained superimposed and compared against the initial efficiency curves or "signature" of the meter under test. The term signature symbolises the uniqueness of one meter curve when compared with another and is a true representation of performance of a meter over its entire operating range within those chosen conditions. A final "signature" test had to be done in order to be able to separate meter readings due to meter deterioration with those attributable to installation conditions. The following chapters describes the research programme and then gives an account of the tests undertaken and of their results.

2 Standards for installation and previous researches

Comprehensive standards have been developed and researches undertaken on measurement of flow in closed conduits, using pressure differential devices such as orifice plates, nozzles and Venturi tubes when they are inserted in conduits running full to determine the flowrate of the fluid. British Standard (BS1042, 1992), and International Standard (ISO5167, 1991) are a few reference examples which specify installation and operating conditions of these devices with a great degree of detail. For volume flowrate methods of measuring cold potable water using meters, International Standard (ISO4064,Part Two,1978) and International Organisation for Legal Metrology (OlML, Document 4, 1981) recognise the need for straight lengths of pipe before and after a meter. The length is given in multiples of the nominal diameter D of the pipe in which the water meter is installed. For both single jet and multijet meters, the upstream and downstream lengths should be 3D and 1D respectively, regardless of the size of the meter. On errors due to installation effects the International Organisation for Legal Metrology (OlML, Document 4, Section 6.3, 1981) admits that "the effect of installation conditions on the accuracy of a water meter has not been comprehensively investigated". A research programme (Harrison, 1990) financed by the European Community used a number of water meter test laboratories

in investigating the effects of flow disturbances on the accuracy of inferential water meters. In this research they developed "standardised in-line flow disturbance devices" to create upstream and downstream velocity profile distortions and upstream and downstream swirls. The conclusion from this research was that flow disturbances change the accuracy of modern water meters, installed in a pipe as stipulated in the OIML document, by more than the permitted amount. This report also references an unpublished KIWA report of August 1976 which has a bibliography of about 12 references relating to the influence of installation conditions on the accuracy of water meters.

3 Domestic water meters

Most domestic water meters are mechanical meters that can conveniently be divided into two main types: (1)Displacement and (2) Inferential. Type 1 comprises meters which are volumetric in operation, the cyclic displacement of the detecting element, e.g. a piston, being directly proportional to the volume of fluid passing through the meter during each cycle. From an academic point of view, displacement meters should be subdivided into positive -displacement and semi-positive displacement types (Fig. 1), the former classification covering those meters which employ a packed piston. When a packed piston is used there is no leakage so that, for all practical purposes, the meter can register down to zero flow. However the modern trend on the design of the displacement meters is to rely on very close machining tolerances between the moving element and its working chamber. Inevitably this means that these meters have a certain minimum flow rate below which inaccurate flow registration results.

The cyclic movement of the piston can be followed from Fig. 2 (a, b, c and d). In position (a) both the inlet and outlet ports are in communication with the inside of the piston, the incoming liquid (shown hatched horizontally) starting the piston off in its semi-rotary movement, and expelling the outgoing liquid (shown hatched vertically) through the outlet port. The liquid on the outside of the piston (shown cross hatched) is in a neutral position, since it is cut off from both inlet and outlet ports, but as the

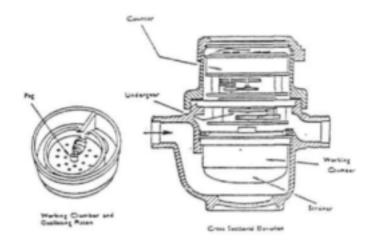


Fig. 1 Semi-positive dispacement meter

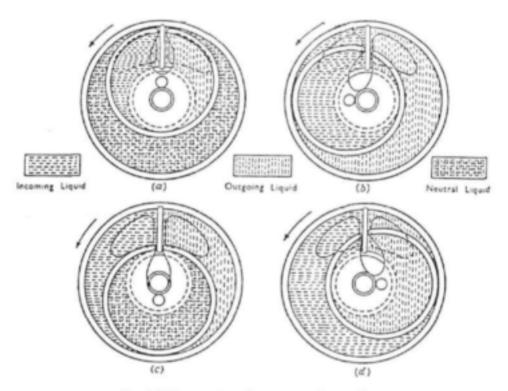


Fig. 2 Piston meter; Sequence of operations

movement of the piston continues it becomes the outgoing liquid, and is discharged through the outlet port. In position (b) the incoming and outgoing liquid is on both sides of the piston, while in position (c)

the incoming liquid is on the outside of the piston, the outgoing liquid on the outside of the piston to the other side of the radial partition being expelled through the outlet port. At this instant the liquid on the inside of the piston is neutral, since it is cut off from both ports, but it becomes the outgoing liquid as the movement of the piston proceeds. The final position (d) shows the piston 90° before position (a). It will be seen that the piston is always moving in the same direction, so no shock is experienced, and each semi-revolution permits a definite volume of liquid to pass through the meter

Type 2 embraces inferential meters; they measure the velocity of flow, and from this measurement infer the volume of flow hence the name inferential meters. In all mechanical meters of the inferential type the moving element consists of the rotor, and the basic principle is to design the meter in such a manner that, over the working range of the instrument, the speed of rotation of the rotor bears a constant linear relationship to the velocity of flow through the meter. The force acting on the rotor is the driving torque which is resisted by the torques due to damping, fluid friction (viscous drag) and mechanical friction. A single-jet (Fig.3) passes the total flow through one jet which strikes the rotor at one point on its periphery. A multi-jet meter (Fig. 4) embodies means for dividing the total flow into a number of jets spaced around the periphery of the rotor.

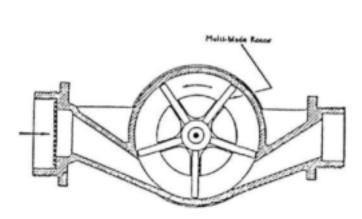


Fig. 3 Single-jet meter

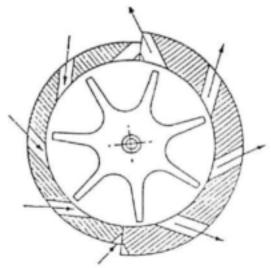


Fig. 4 Multi-jet meter

Domestic meters commonly used are the inferential (single-jet and multi-jet) and volumetric (piston) meters with the following nominal bores commonly used; 15 mm, 20 mm and 25 mm. This is because of the relatively low draw-offs at which water enters into consumer networks. For pipeline systems that have very high variances in flow rates such that none of the operating ranges of the flow rates of the above mentioned meters is adequate, larger meters and combination meters have been developed but these are mainly for industrial and zone water metering.

Most households have moderate flow rates and therefore the 15 mm, class B meter is the most common meter installed and hence it was used for the research. Whether a volumetric or inferential meter is installed is purely a matter of choice of the water authority or contractor, but can be restricted by whether the meter is to be installed horizontally or vertically. Most inferential meters are horizontal meters but most volumetric meters can be used in both the horizontal and vertical installations.

4 Calibration standards and terminology for water meters

All water meters with a nominal bore not exceeding 100 mm are calibrated for compliance with South African Bureau of Standards (SABS1529-1,1994), and are metrologically classified as A, B, C or D depending on the level of accuracy required from the meter. The least accurate is a class A meter which is not used for billing purposes. The most accurately calibrated meter is a class D meter which has also the largest range (see Table 1 below) although for purposes of billing the use of classes B and C have tended to dominate with the former being commonly used by both domestic and commercial users. Consequently the meters used in the research were class B meters as they are commonly used for domestic metering and consumer billing.

A calibrated water meter has a flow range in which it is designed to operate ranging from a minimum to a maximum flow rate. The minimum flow rate q_{min} is the lowest flow rate at which the meter is

Table 1-Metrological class of meters

1	2	3	4	5	
Class of meter	For q_p not exc	ceeding 10m ³ /h	For q_p exceeding $10\text{m}^3/\text{h}$		
	Minimum flow rate q _{min}	Transitional flow rate q.	Minimum flow rate q _{min}	Transitional flow rate q	
A B C	0,04 q ₀ 0,02 q ₀ 0,01 q ₀ 0,0075 q ₀	0,1 q_p 0,08 q_p 0,015 q_p 0,0115 q_p	0,08 q p 0,03 q p 0,006 q p	0,3 q _p 0,2 q _p 0,015 q _p	

required to give indications within a permissible tolerance whereas the permanent flow rate q_p is the flow rate for which the meter is designed and at which the meter is required to give indications within the permissible tolerance under normal conditions of use. The transitional flow rate q_t occurs between the permanent flow rate and the minimum flow rate. This is divided into two zones, the upper zone and the lower zone, each characterised by a specific permissible tolerance. The overload flow rate q_t which is twice the permanent flow rate is the highest flow rate the meter is required to operate in a satisfactory manner for a short period of time without deterioration.

5 Flow parameters that affect a meter

For both inferential and volumetric meters, the diameter of the main pipe bears little relationship to the nominal size of the meter which should be used. Each nominal size of any particular make has a definite minimum flow, below which it will not register accurately, and a maximum flow rate, above which it will be overloaded. Hence the size of the meter selected will depend entirely on the anticipated flow range. The exception to the above statement, in so far as the low flows are concerned, is the positive type meter, which, as already explained, is accurate to what is, for all practical purposes, zero flow.

Both the volumetric and velocity meters derive their driving energies from the fluid which they are measuring, hence some flow parameters which affect this energy do influence the accuracy of these meters. It has been found that the following parameters affect the accuracy of a meter;

- (a) the upstream velocity profile distortion,
- (b) the temperature effect ,
- (c) the viscosity effect, and
- (d) the swirl effect.

It was also found that the meter characteristics is a function of the velocity profile just upstream of the rotor. The volumetric meters have indicated in previous researches (Harrison, 1990), (OIML, Document 4, 1981) to be insensitive to upstream velocity profiles as well as the swirl effect. Temperatures and viscosities of potable water as tested in the laboratory can be strictly controlled, therefore their effects on the systematic errors of the meter readings are constant.

Fittings, bends and valves before a meter introduce either swirl or velocity profile distortions, as well as introducing more head losses. It is therefore worth investigating for each type of meter the effects of these on the accuracy of the meter. Caution is needed in separating the errors due to air pockets and general errors characteristic with each test rig from those inherent in the flow due to fittings. Air pockets are inherent in many actual ground installations although use of rising mains and air release valves can minimise these. Whereas test benches can be vacuumed (this is the ideal condition) but normally merely flushing the entire system by fully opening the downstream valve to the meter under test removes most of the air pockets. A much more recent practice on some test rigs without vacuum pumps on conventional meters is to invert them 80° from the normal horizontal position and flush water through, expecting all air to rise and be flushed out.

6 Research equipment

The details on models of inferential and volumetric meters used in the research are shown in Table 2 below. Three meters were disqualified after the initial signature test as they did not comply with South African Bureau of Standards (SABS1529-1, 1994) tolerances against which they were type approved and therefore could not be taken to be representative of other meters. There was no criteria used in selecting any particular brand of meters as these meters were donated by the respective meter manufacturers. The first column of the table identifies the meter model, the calibration class, the nominal operating pressure of the meter and the pressure loss across the meter at q_s. The second column identifies the nominal size of the meter in volume flowrate and the type (whether volumetric or inferential) and the way it is installed (horizontal or vertical). The fourth column describes whether the meter is type approved for trade use in South Africa and the thread size of end connections.

The SABS water meter laboratory used in the research handles all type approval, production verification and dispute testing of water meters. Copies of the calibration certificates of the 100 # and 10 # tanks used for measuring the actual volume of water are shown in annex B. Thus the volume measured from these tanks is the meter prover volume used in determining the error. Its calibration therefore can be traced to the national standard via the Weights and Measures Act , vis -a-vis, the Trade Metrology Act, (Act 77 of 1973), of South Africa.

7 Methodology

The meters were tested in three batches owing to test bench limitations and because meters of different types cannot be tested together. For example, volumetric meters cannot be tested together with inferential meters. The three batches were;

Batch 1 consisting of inferential meters from models C, D and E,

Batch 2 consisting of volumetric meters from models B and F, and

Batch 3 consisting of inferential meters from model A only.

Table 2 - Meters used in research

1	2	3	4
Meter Model	Size and type	ID Number	Remarks
Model A Class "B" PN16, P = 100 kPa	1,5 m ³ /h inferential horizontal	Al1 Al2 Al3	Type approved Connection size = G 20 B.
Model B Class "B" PN16, P = 100 kPa	1,5 m ³ /volumetric horizontal and vertical	BP1 BP2 BP3	Type approved Connection size = G 20 B
Model C Class "B" PN16, P = 100 kPa	1,5 m ³ /h inferential, horizontal	CI1 CI2 CI3*	Type approved. Connection size = G 20 B In plastic body
Model D Class "B" PN16, P = 100 kPa	1,5 m ³ /h inferential, horizontal	DI1 DI2 DI3*	Type approved. Connection size = G 20 B In brass body
Model E Class "B" PN16, P = 60 kPa	1,5 m³/h inferential horizontal	Ei1 Ei2 Ei3*	Type approved. Connection size = G 20 B
Model F Class "B" PN16, P = 40 kPa	1,5 m ³ /h volumetric horizontal	FP1 FP2 FP3	Not type approved. Connection size = G 20 B

Tests were conducted within 10 % of the specified flow rates q_{min} , q_1 , q_2 and q_5 , in accordance with International Standard (ISO4064, 1983) and South African Bureau of Standards (SABS1529-1,1994), for all the tests except for the initial and final signature tests, where intermediate and extreme low and high flow rates were chosen in addition to those mentioned above.

As mentioned earlier, the initial signature tests were carried out on all the meters with a total of twenty two flow rates over the full range of the meter. The meters were installed with standard connectors on the normal manifold used for type approval of meters. The configuration is shown in Photograph 1 in annex C. Long straight lengths of pipes greater than 3D on the inlet and greater than 1D on the outlet of each meter ensured fully developed flows entering and undisturbed flows leaving the meter. The identification numbers and the route, which is the relative identification of each meter on the test bench counting from the inlet of the test bench, were recorded on the test sheet. This ensured that a meter

was always installed in the same position relative to other meters in every configuration under test. Once on the test bench, air was removed by flushing with water by opening the downstream valve until no more bubbles could be seen through the graduated sight glass of the variable area flowmeter. The initial reading after flushing was recorded for each meter and then by carefully adjusting the downstream ball valve to the required flow rate, the first test run could be started. By switching on the solenoid valve integral with the variable area flowmeter connected to a timer which automatically switched off when the volume of the measuring tank had been filled, a test run could be completed and the results recorded. The volumes were read from a scale on a transparent sight glass attached to the tank. The temperature and pressure of the water were read from dial gauges installed upstream of the meters. The water coming from a constant head tank on the roof of the eighth floor (about 325 kPa static head) of the building ensured that a constant pressure for each flow could be maintained. The readings on the meter were then recorded and by subtracting the initial reading taken before the test, the volume of water as recorded by each meter were noted down. Three readings were taken for each chosen flow rate. The percentage error was then calculated from the following formula:

Percentage error of meter reading =
$$\frac{V_{\text{meter}} - V_{\text{tank}}}{V_{\text{max}}} \times 100$$
 (1)

where

V_{meter} is the volume of water as read by the meter;

V_{tank} is the volume measured from the tank (meter prover volume).

Thus the technique involved the determination of systematic and random errors and uncertainties for each stage in the measurement chain. Minimizing systematic errors was achieved by setting up the bench properly, for example, pipe alignments of the system ensuring stresses were not transferred from the pipework to the meter under test. Random errors were minimized by doing three tests at each chosen flow rate within short periods of time or consecutively to prevent the effect of wear and

tear or environmental changes. This emphasized the significance of the final efficiency test as an indicator of the extent of the increase of error due to wear and tear.

The results were entered into a spreadsheet (see annex E) with formulas including (1) above, which calculated the average value of the error over the three readings taken for each flow. The spreadsheet also calculated the percentage variance of each reading from the average and this indication of the scatter of batch readings was used to separate significant random errors in meter reading caused by the technician from those attributable to the meter. Graphs of the percentage error versus the flow rate (see annex C) were then plotted for all the meters. Because of the periodic non-availability of the laboratory in order to accommodate other tests, the meters had to be stored for some days before tests could continue. In such cases all meters were fitted with plastic endcaps at their inlets and outlets to prevent the ingress of dirt. In addition plastic meters were filled with water to ensure that the plastics did not dry out which could result in additional errors.

7.1 Ball valve configuration

This test involved inserting a 15 mm PN25 ball valve which complied with South African Bureau of Standards (SABS1056-3,1985), before the inlet of each meter (Fig. 5 below and photograph 2 in annex C). The following adjustments to the valves were then made:

- (a) fully open valve;
- (b) 22,5° open valve; and
- (c) 45° open valve.

The effect of these adjustments was to introduce a velocity profile disturbance which disrupted the steady flow. This is a common practice in meter box installations and is recommended in some guidelines shown in annex A on Some Common Installation Practices. Different valves are used by different meter manufacturers and produce different flow distortions, hence results obtained were

for these types of ball valves only. Seven flow rates were chosen for each valve position and readings recorded three times for each flow rate. The results of these tests were entered in spreadsheets and the graphs obtained were superimposed on the initial signature curve of the respective meters.

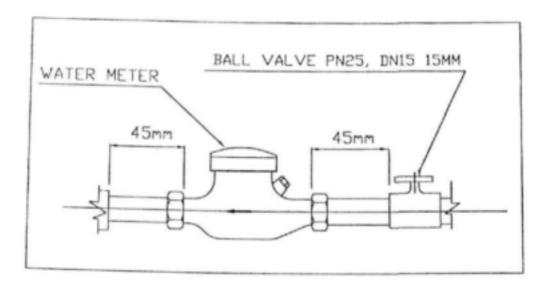


Fig. 5 Ball valve configuration

7.2. 45-degree tilt configuration

This test involved setting up the meters on the normal test manifold and then rotating the meters by 45° from the vertical (Fig. 6 below and photograph 3 in annex C). This is not a standard practice but due to its prevalence in the field, it was decided to investigate its influence on meter accuracy.

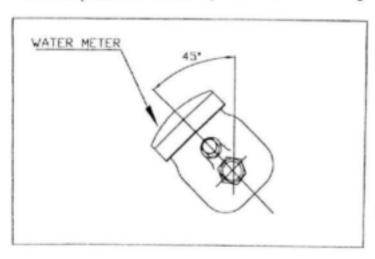


Fig. 6 45° degree tilt configuration.

The angle of inclination from the vertical could vary from 0° upwards, but due to the limited time and resources available, the worst case was investigated. Seven flow rate readings were taken for all the groups of meters and the results plotted against the initial signature curve of the respective meters

7.3 Above ground configuration

This test involved assembling galvanized fittings to form a typical above ground installation (Fig. 7 and photograph 4 in annex C) but without the inlet gate valve. The valve was omitted deliberately to ensure that the influence of the galvanised elbows and fittings could be investigated alone. This installation is quite commonly used and typical practical applications are depicted in Annex A in drawings by the Department of Water Affairs and Forestry and the City Council of Pretoria. Seven flow rates were chosen for each group of meters and the resultant curves superimposed on the initial signature curves of the respective meters.

Finally, the meters were set up again on the normal test manifold and the twenty flow rates repeated for the meters. A final signature test was done for all the batches of meters and again the resultant curves were superimposed on the initial signature curves of the respective meters.

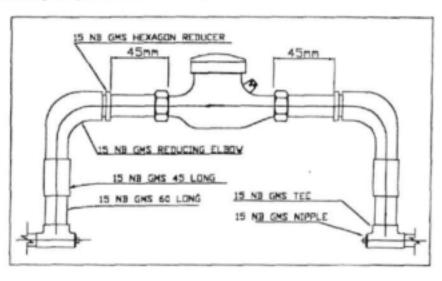


Fig. 7 Above ground configuration

8 Results of tests and discussion

Each meter had two graphs plotted consisting of:

- (a) one graph with the test curves of the results obtained with a ball valve in various stages of opening superimposed on the initial signature, and
- (b) a second graph with curves for the results obtained with the meter rotated 45° from the vertical and the above ground installation superimposed on the initial and final signature.

The two set of graphs for each meter are shown in Annex D.

8.1. Model A (Al1, Al2, Al3)

From the graphs of the three meters tested in the Model A group—all the curves had peaks at a flow rate of 500 i/h on the initial efficiency curves. Meter Al3 failed to meet the SABS tolerance at this point. However, as the repeatability of the meters was the same, no meter was disqualified. The curves with the valve in various positions of opening crept upwards by not more than 2 % from the initial curve except at flow rates greater than q_p where the reverse was true. There was very good correlation with the initial and final curves for all the test configurations except for the 45° orientation where all the meters severely underregistered increasingly from 200i/h to q_{min} . Therefore, it was conclusive from the tests that the 45° orientation affected the performance of the meter.

8.2 Model B (BP1, BP2, BP3)

There was good correlation of all curves versus the initial and final curves at flow rates greater than 200 t/h (all turning points of the curves appeared here), as expected for a volumetric meter. Below 200 t/h variances from the initial efficiency curve were greatest for the 22,5° open configuration (about 1% underregistering), whereas the fully open configuration correlated well. The final signature shifted steeply below 100 t/h resulting in failure to meet SABS tolerance. Hence the results were not conclusive and could not be attributed to the fittings or configurations.

8.3 Model C (CI1, CI2, CI3)

The initial signature curves showed the meter CI3 having two peaks; one of overregistration at 1,5 m 3 /h and one of underregistration at 2 m 3 /h. The peaks were outside the SABS tolerance band and not similar to the other curves from the other two meters, this meter was rejected. The 45 $^\circ$ orientation produced the same effect as in the other inferential meters in that the curves steeped extremely giving severe underregistering at flow rates less than the transitional flow rate. The other configurations had small variances from the initial and final efficiency curves, although the fully open valve configuration on meter CI2 curve near q_{\min} is uncharacteristic and cannot be easily explained. Hence the only notable effect was with the 45 $^\circ$ orientation to the vertical as the erratic curves of the other configurations did not reveal conclusive trends.

8.4 Model D (DI1, DI2, DI3)

A similar initial signature curve characteristic to the one from meter CI3 above resulted in meter DI3 being rejected. The curves with valve configuration show very close correlation between the curves at all positions of opening and hence there was no considerable effect on the meter accuracies. Nothing could be concluded from the rest of the tests as the meters started showing what seemingly appeared to be counter problems. Hence no conclusion could be drawn from this model of meter. The counter is a mechanical part of the meter which counts the volume of water by way of converting the revolutions of the turbine or piston shaft, through a gear train transmission into cubic meters. Roller or drum counters are used for depicting tens, hundreds and larger volumes in cubic meters whereas circular graduated dials are used mostly for fractions of a cubic meter.

8.5 Model E (EI1, EI2, EI3)

The initial signature curve for El3 was uncharacteristic when compared with the other two meters of the same model hence this meter was rejected. The 45° orientation produced the same trend as in other inferential meters but the pitching of the error curves began much earlier at around 750 i/h. The rest of the configurations correlated well with the initial and final signature curves.

8.6 Model F (FP1, FP2, FP3)

All the curves of the various configurations of all the meters correlated satisfactorily with the initial and final efficiency curves at almost all flow rates except for small kinks at 200 i/h for the fully open valve configurations for meters FP2 and FP3. It is with repeatable results of such meters that definite conclusions can be drawn about the performances of volumetric meters as there were no peculiar and inexplicable meter performances. Thus for these meters it can be safely concluded that they were not affected by any of the test configurations.

9 Conclusion

9.1 Conclusions of research

The investigation of the influence of various fittings on the accuracy of a meter produced various meter performances and results. The main finding of this research was that at an installation of 45° to the vertical an inferential meter severely underregisters the value of the water passing through it. All the inferential meters had large shifts from the signature curves at flow rates below the transition flow rate. Tests carried out on this configuration showed the curve of every inferential meter deviating towards errors greater than 10 % at flows near the minimum flow rate. The presence of a valve upstream of both inferential and volumetric meters shifted the error curve marginally from the signature curves and therefore did not affect their accuracy severely.

The above ground fittings did not displace the curves large enough for both types of meters tested to enable drawing of any conclusions. The piston meters proved that some models were sensitive to upstream flow conditions and orientation from the vertical and other types were not. The model F piston meters were hardly affected by any configuration tested whereas the model B meters had

inexplicable large displacements from the initial signature at flow rates below q_1 . The final signature curves for the latter model also shifted above the SABS 1529-1 tolerances of 5 % at the flow rates near q_{min} , hence it is premature to conclude whether the fittings affected the meter or that the meter accuracies had deteriorated due to wear and tear.

Other recommendations that emanated from this research are:

- An inferential meter designed to operate in the horizontal standard position should always be installed with its turbine shaft axis coaxial with the vertical axis. More so there is need to investigate the critical angles or angular tolerance to which different models of meters start to lose sensitivity.
- The above ground installation does not impart large inaccuracies on meter performances and its use in meter installations where ease of reading is required, can still remain a normal practice.
- That an inlet ball valve of the type used in this research does not impart large inaccuracies on domestic meter performances. Emphasis is put on the words "type used in this research" as different valves impart different flow disturbance characteristics and therefore more types of valves should be tested.
- Better training curricula should be formulated for all plumbers to avoid improper installation
 of meters and increase their understanding of the importance of the information derived from
 a water meter in local government water management systems.
- Regular checks on meter manufacturers should be continued long after type approval to

ensure that they still produce their meters with accuracy and durability as key requirements.

This recommendation emanates from the fact that some type approved meters used in the research, failed the initial selection criteria.

 All municipalities and water governing bodies, plumbers institutions and other interested organizations should make use of the "Guidelines on Domestic Meter Installation Practices" which emanated from this study.

9.2 General conclusions

The problems that arose due to the suitability of some of the meters chosen as standard comparison meters brought to the research another interesting observation on meters that are already type approved under the existing South African Bureau of Standards (SABS 1529-1,1994). The meters CI3, DI3 and EI3 were disqualified from the research as they failed to meet the tolerances specified in the above-mentioned standard. The meter AI3 failed throughout all the tests at 500 i/h and the other two meters from this type had kinks of overregistration on the curves at this flow rate which resulted in meter AI2 exceeding the 2 % error stipulated by the specification.

The explanation for the severe underregistration at lower flowrates for inferential meters on the 45° orientation can be due to the increase of the mechanical friction between the rotor and the shaft bearings as the points of support of the rotor are no longer the bearing areas only as designed. As mentioned earlier the force acting on the rotor is the driving torque, which is resisted by the torques due to damping, fluid friction (viscous drag), and mechanical friction. For a fluid of constant density such as water, the driving torque is proportional to V², where V is the velocity of flow (relative to the rotor blades), the damping torque is proportional to N², where N is the speed of rotation of the rotor, the torque due to fluid friction is proportional to V² and the torque due to mechanical friction is proportional to the weight of the rotor normal to the point of support. If the damping and fluid friction torques are

large in relation to the mechanical friction torque, the speed, N, of the rotor will be directly proportional to the velocity of flow, V, and accurate metering will result. Therefore, the torque due to mechanical friction must be kept low, and this can be done only by careful design of the rotor bearings and reducing to the lowest possible limit the transmission load to the presentation element. The coefficient of friction between the rotor and the shaft can increase due to improper seating of the rotor bearing on the shaft bearing. This will mean high mechanical friction and consequent underregistering at lower flowrates. As the velocity of flow increases above transition region the rotor is floating completely in water and there is minimal contact of its bearing surface with the bearing tip of the shaft. Therefore the reduced mechanical friction resulted in accurate metering at higher flowrates for all meters irrespective of the 45° tilt.

10 Recommendations for future research

The main recommendation for future research is that more tests should be done on most sizes of both single-jet and multi-jet inferential meters simulating most existing installation practices in order to be able to make comprehensive conclusions. As these researches would involve numerous tests, more laboratories can be drawn into these researches and intercomparisons done initially to be able to establish compatibility in the results of the same meters. A large enough statistically representative sample of meters is necessary for these kind of tests bearing in mind that some meters fail to perform and have to be removed from a research. As technology is moving towards electronic meters, most research is going to shift towards these meters. However, as the electronic meter can only be as accurate as the mechanical meter that transmits the source signal, it is recommended that these researches be continued and accelerated. The unusual phenomena exhibited by some volumetric meters should be investigated further as there was ambiguity in the results recorded for the piston meters tested. Lastly, most of the meters exhibited abnormal characteristics which might have been caused by entrained air, hence research into the effect of air on the accuracy of domestic meters is recommended.

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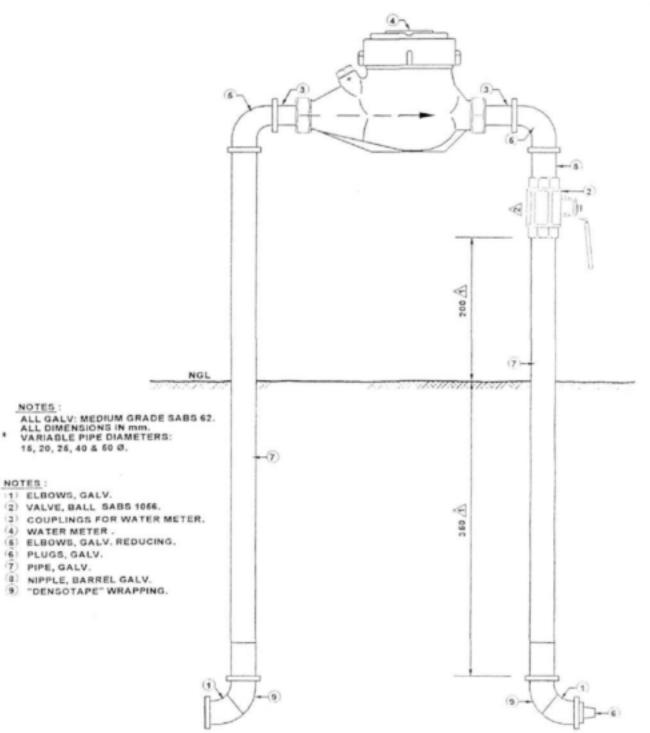
SOUTH AFRICAN BUREAU OF STANDARDS SABS 1529-1(1994)Water meters for cold potable water - Part 1: Metrological characteristics of mechanical water meters of nominal bore not exceeding 100 mm.

SOUTH AFRICAN BUREAU OF STANDARDS SABS 0306 (1999) The management of potable water in distribution systems.

SOUTH AFRICAN Water Services Act (1997) Act 108.

ANNEX A

Some common installation practices

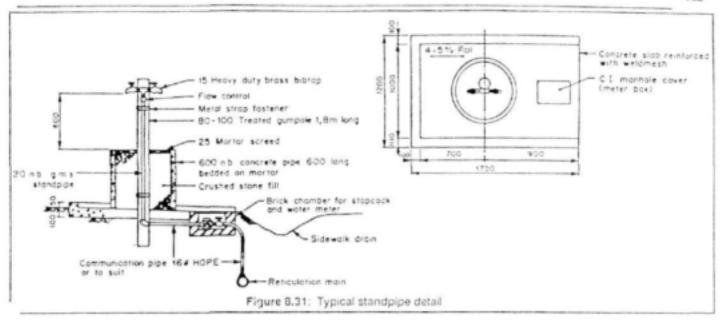


NOTES:

NOTES:

WATER METER CONNECTION DETAIL N.T.S.

**	AMENDMENTS - WYSIGINGS	DATUM	DEDGRED ORTHERP	WATER & THE ENV		STADSRAAD V EPT. WATER &	AN PRETORIA DIE OMGEWING
1	CIMENTIONS REVISED	8/99	L. VILJOEN	WATER S	UPPLY	MISCELLA	NEOUS
2	VALVE POSITION CHANGED (P. DE KLERK)	5/93 TRACED MADEINEK 8858/W/2		TYPICAL STANDPIPE FOR 150, 200, 250, 400 &			
			CHECKED MAGESTRA	50g WATER CONNECTION			
			T.F. WESTMAN	CHIEF WATER ENGINEER	GFF ENGINEER	CONTRACT NO.	GRANING No.
			OCTOBER 1995	PHS CRONJE Pr.Eng	NDe V LOUBSER Pr.Eng	ADMINAN IN	8858/W/2



An acceptable discharge capacity from a standpipe is about 15 l/min per tap. For commonly used taps the calculated discharge range, at an assumed efficiency of 80 % is:

Tap diameter	Dischar	ge
	5 m head	60 m head
15 mm	8 l/min	75 l/min
20 mm	14 l/min	140 l/min

However, the high discharge rates for a 60 m head will normally be reduced by the limitations of the pipework. In practice, measured flow rates to single dwelling houses seldom exceed 40 l/min.

Water taps with high capacities may result in large water wastage when taps are left open, even for only a short time. Therefore tap capacity should be restricted to a maximum of 20 l/min. Figure 8.31 gives details of a typical standpipe installation.

Water klosks are being used extensively in the semi-formal settlement areas where urbanisation has caused the rapid growth of settlements. The sale of water at klosks provides an effective means of recovering costs; this is especially relevant where community management structures are not yet in place.

Due to their higher cost and the need for sufficient users to make individual units commercially viable, klosks are usually spaced further apart than standpipes would be. For the system to be viable, individual klosks should supply at least 50 dwellings.

Facilities for accurately measuring and dispensing the standard purchase volume (usually 20 or 25 litres) should be provided. The structures should be sturdily constructed, and have lockable facilities.

Water tanks with a tap may be the first level of supply improvement before any distribution piping is installed. Water may be supplied to the tank by a road tanker, by gravity flow from a spring, from a borehole equipped with an engine-driven pump, by rainwater, or from a small treatment works. People may need to walk long distances to the tank to collect this water. However, its quality is usually good, and it may often be the only source of water available to a community.

Where the tanks are filled by rainwater collection, it is possible for each home to own its own tank and maintain its own systems. It is important to set up a committee of local residents to manage any such system for public supply.

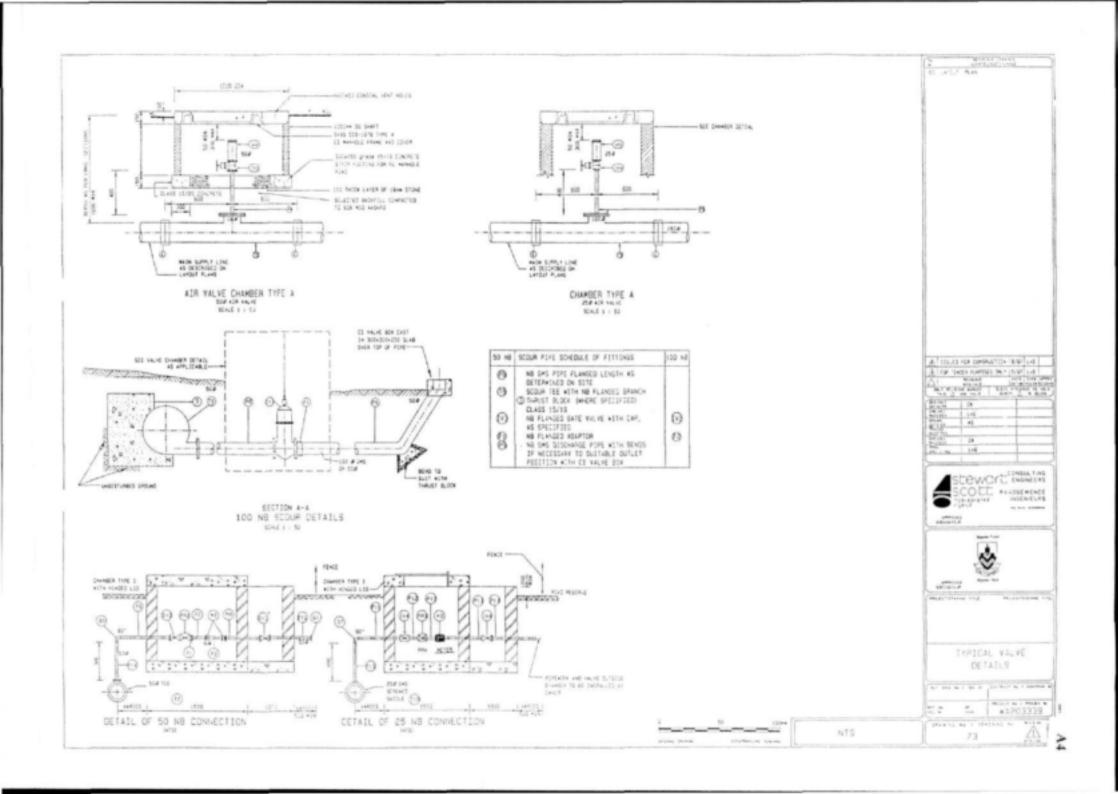
The size of the tank and its design should be in accordance with the design principals given elswhere in this document.

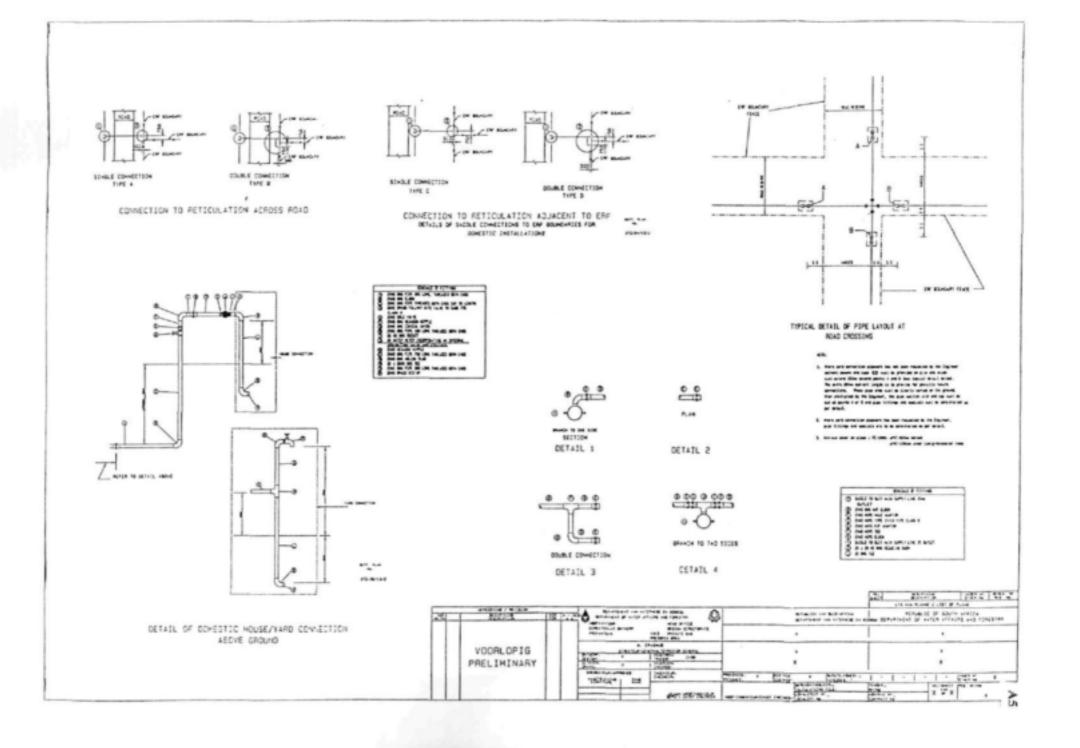
Water vendors are not generally considered in the planning stage, and may often resist the upgrading of a water supply. These entrepreneurs often operate with only a donkey can and a number of 200 litre drums, or with motorised transport.

Table 8.19: Selection criteria for water supply terminals

	Attordability (Investment)	Cost recovery	Maintenance needs	Unit cost
Public standposts	medium	flat rate	medium	low
Water klosks	medium	per amount used	low	high
Tanker supply to tank	medium	flat rate	medium/high	medium/high
Vendors	low	per amount used	low	medium/high
Metered yard tap	high	per amount used	low	low
Metered house connection	high	per amount used	low	low
Handpump	medium/low	flat rate	medium	medium
Spring supply to tank	low	flat rate	low	low

Chapter 8 page 34 Water supply







a) Pretoria - Meter installed with upstream bends



b) Pretoria - Meter installation tilted



c) Pretoria - Meter installed with upstream bends



d) Pretoria - Meter installation tilted



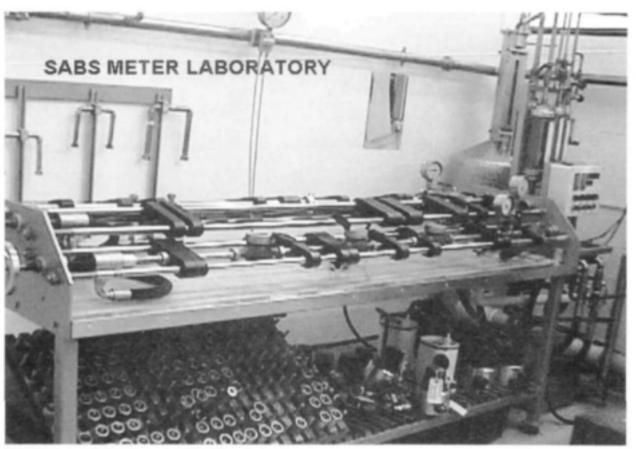
e) Pretoria - Meter installed in a skew pipe arrangement



f) Pretoria - Meter installed with upstream bends

ANNEX B

SABS water meter laboratory and calibration certificates



SABS Water Meter Accuracy Test Bench





South African Bureau of Standards, Private Bag X191, Pretoria, 0001 Tel: (012) 428-7911, Fax: (012) 344-1568

South African National Accreditation System
Accredited Laboratory No.

Tel No: (012) 428-7014 Fax No: (012) 428-6552

1405

Certificate of Calibration

No.

198/98

This certificate is issued in accordance with the conditions of the approval granted by the South African National Accreditation System. It is a correct record of measurements made. Copyright of this certificate is owned jointly by SANAS and the SABS. This certificate may not be reproduced other than in full, except with prior written approval of SANAS and the SABS.

ON SITE CALIBRATION

Calibration of

: Volumetric measures.

Description of item/s

: 1 x 100 @ volumetric measure/s. 1 x 10 @ volumetric measure/s.

Calibrated for

Fluid Technology Division Attention: Mr J Wantenaar

Room M025 SAB3

Calibration procedure Date of calibration See page 2 par. 2

1998-06-26

Validity of calibration : The value/s in this certificate is/are correct at the time of calibration.
Subsequently the accuracy will depend on such factors as the care exercised in handling and use of the instrument/s and

handling and use of the instrument/s and the frequency of use. Recalibration should be performed after a period which has been chosen to ensure that the instrument's accuracy remain/s within the desired

limit/s.

Calibrated by

SG Mahalngu

Checked by

BF vd Merwe

Page 1 of 2

CALIBRATION CERTIFICATE NO. 198/98

1.	Laboratory Standards and Equipment	SABS No.	Cert.No.
	5 & strike measure	NCS 5	231/NCS 5/97
	50 & volumetric measure	23529	231/23529/97

2. Procedure

The volumetric standard was calibrated using the volumetric method (direct volume to volume). Corrections to the apparent volume of water were made for the differential water temperature and thermal expansion of the material of the volumetric standard. Quality Procedure/s QP/231/14.

3. Results

Serial No.	Graduation calibrated in £	Actual volume at 20 °C in &	Uncertainty of calibration in 2	
WSM 963610	10	10,00	± 0.02	
WSM 963609	100	99,99	± 0,07	

4. Remarks

A drainage time of 15 seconds was used during the calibration. The coefficient of cubical expansion of the volumetric standard calibrated was assumed to be: 0,0000507 &/°C.

Measurements were made at a 95 % confidence level.

Calibrated by

SG Mahlangu

Checked by

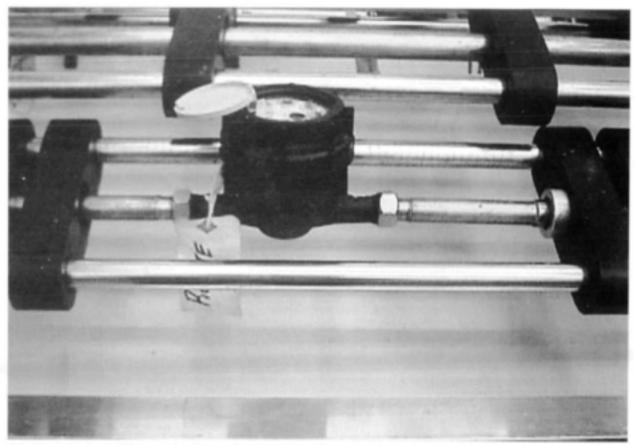
: BF vd Merwe

:

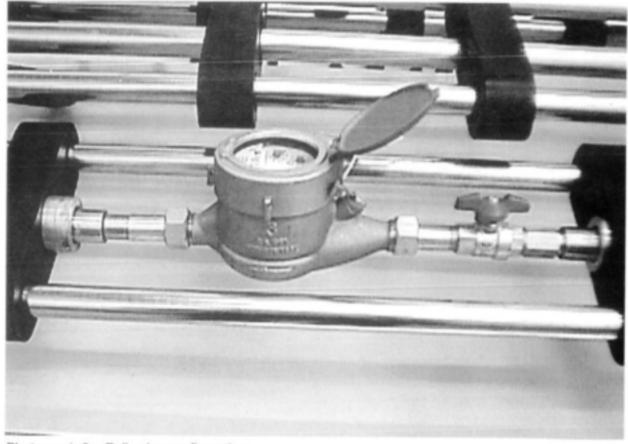
Page 2 of 2

ANNEX C

Photographs of test configurations



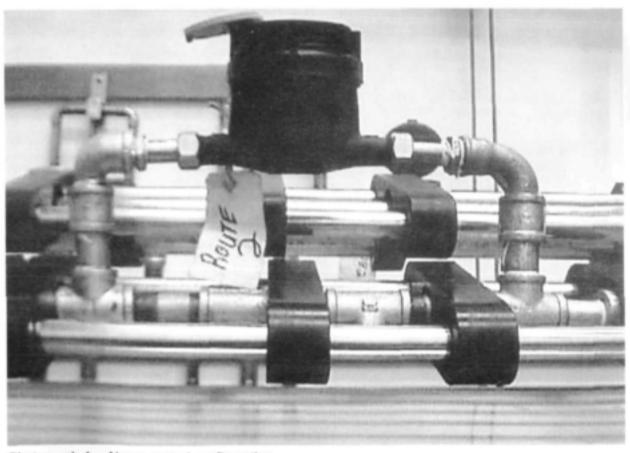
Photograph 1 - Initial and final signature configuration



Photograph 2 - Ball valve configuration



Photograph 3 - 45-degree configuration



Photograph 4 - Above ground configuration

ANNEXURE D

Examples of graphs generated for different types of meters:

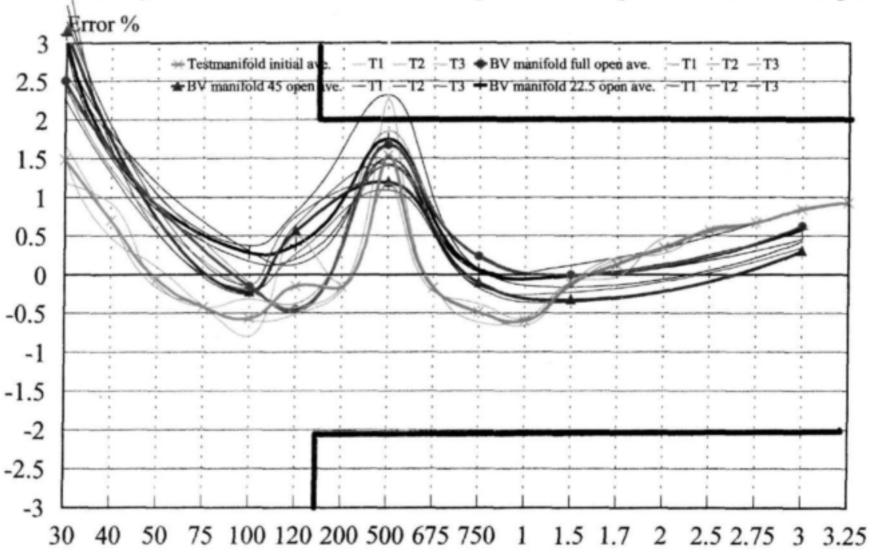
D₂ & D₃ = Inferential meter with readings reflecting all the tests and positions.

D₇ & D₉ = Piston meter with readings reflecting all the tests and positions.

(Please note that a large number of graphs had been generated by the study. Should the reader require a full set, then kindly contact WRC in this regard.)

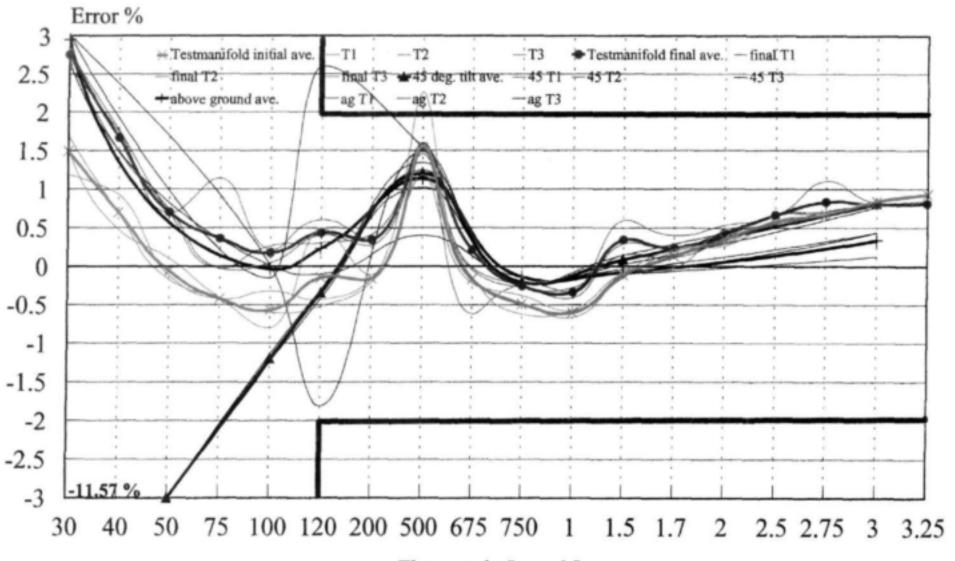
Domestic Water Meter Model AI 1 Qp = 1.5 m3/h WRC Project

Efficiency Curve SABS 1529 - 1 1994 full & partial flow range & various manifolds/positions



Domestic Water Meter Model AI 1 Qp = 1.5 m3/h WRC Project

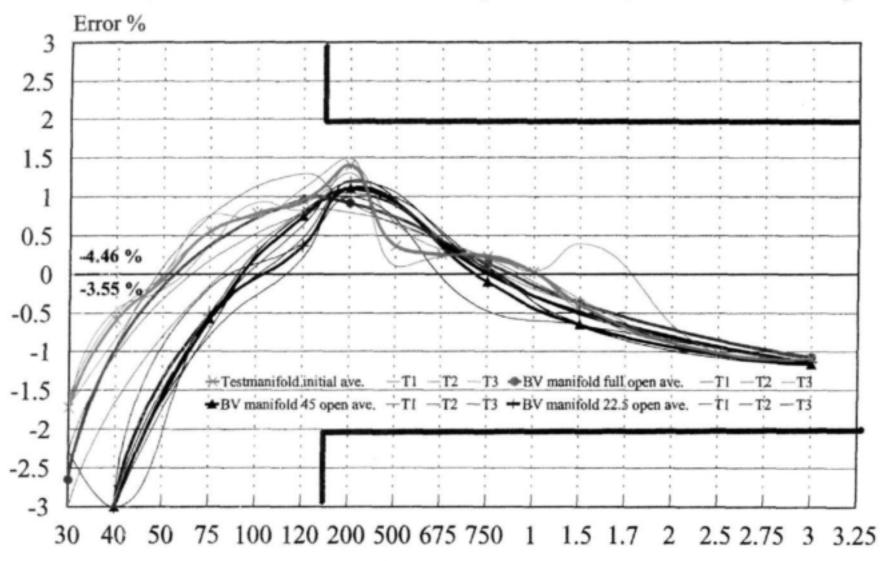
Efficiency Curve SABS 1529 - 1 1994 full & partial flow range & various manifolds/positions



Flowrate ltr/h - m3/h

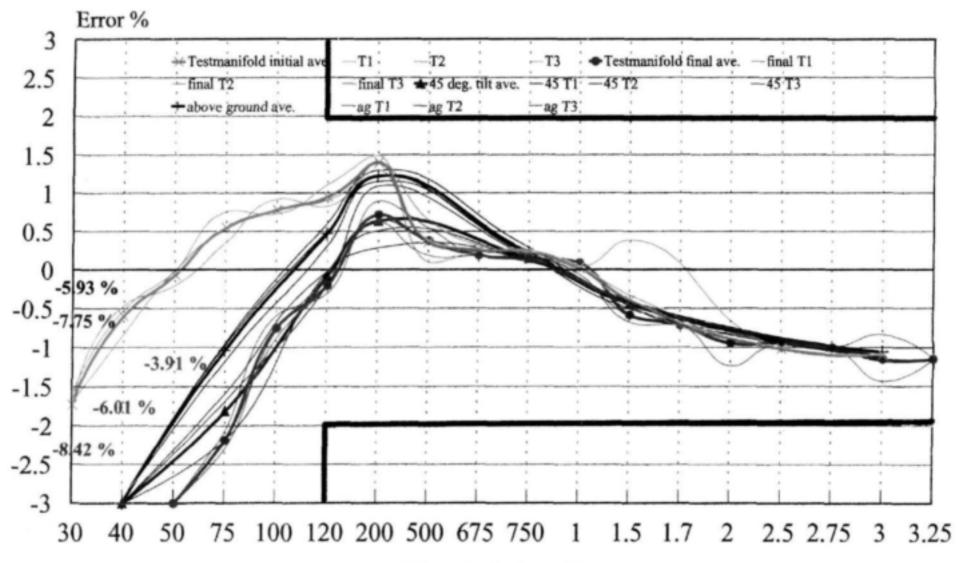
Domestic Water Meter Model BP 1 Qp = 1.5 m3/h WRC Project

Efficiency Curve SABS 1529 - 1 1994 full & partial flow range & various manifolds/positions



Domestic Water Meter Model BP 1 Qp = 1.5 m3/h WRC Project

Efficiency Curve SABS 1529 - 1 1994 full & partial flow range & various manifolds/positions



ANNEX E

Spreadsheets analysis of results

Applicable Regulation SABS 1529-1 1994, section 6.4 and A 4.2h

Meter Size: Meter Class: Magnetic drive

Receipt reading:

Route No:

"3", Qp = 1,5 m3/h
"B"

No 3 Test type: Customer : Manufacturer:

Meter Type:

WRC Project WRC Print date: Print time: 24 March 2000 02:34:41 PM

Revised 16:06/99
File No.: WRCsig-4.rex
Report No.: 3571/930507/R29
Test No: 992102

Flow orientation: P Group: Working Pressure:

Model:		Work	dng Pressure:			
Meter Serial #	Model AI 1		Test # 1	Test#2	Test # 3	aver. 1 -3
Test bench position			# 3	11 3	#3	
	Flow pressure k	Pa	330	330	330	330
	Water temperature	oC	19.0	18.5	18.5	18.1
	Test duration 8	ec .	3059	3235	3373	322
	Volume displacement	ltr	10,022	10.022	10.018	
10 l/h	Start reading m	13	16.43381	16.44411	16.45439	
	End reading m	13	16:44411	16.45439	16.46459	
	Difference	tr	10.30	10.28	10.20	10.26
	Difference	96	2.77%	2.57%	1.82%	
	Actual flow rate ltr/h	our	11.79	11.15	10.69	
ideal <+= 0.5 %	Variance to average		-0.39%	-0.19%	0.57%	

	Flow pressure kPa	330	330	330	330
	Water temperature oC	19.0	19.0	19.0	19.0
	Test duration sec	2273	2158	2316	
	Volume displacement 1tr	10.024	10.025	10.024	10.024
15 l/h	Start reading m3	16.43239	16.41286	16.42334	
	End reading m3	16.41286	16.42334	16.43381	
	Difference Itr	10.47	10.48	10.47	10.47
	Difference %	4.45%	4.54%	4.45%	4.48%
	Actual flow rate ltr/hour	15.88	16.72	15.58	16.05
ideal <+- 0.5 %	Variance to average	0.33%	-0.06%	0.03%	Pass

deal <+- 0.5 %	Variance to average	0.90%	-0.10%	0.09%	Pass
	Actual flow rate ltr/hour	19.08	18.42	20.24	19 22
	Difference %	4.40%	4.50%	4.31%	4.40%
	Difference ltr	10.47	10.48	10.46	10.47
	End reading m3	16.33145	16.39193	16.40239	
20 l/h	Start reading m3	16.37098	16.38145	16.39193	
	Volume displacement ltr	10.029	10.029	10.028	10.029
	Test duration sec	1892	1960 -	1784	1879
	Water temperature oC	19.5	19.5	19.5	19.5
	Flow pressure kPa	335	330	330	332

ideal <+- 0.5 %	Variance to average	0.93%	-0.07%	0.03%	
	Actual flow rate ltr/hour	21.32	21.84	22.31	21.82
	Difference %	3,71%	3.81%	3.71%	3.74%
	Difference ltr	10.40	10.41	10.40	10.40
22.5 l/h	End reading m3	16.35017	16.36058	16.37098	
	Start reading m3	16.33977	16.35017	16.36058	
	Volume displacement ltr	10.028	10.028	10.028	10.028
	Test duration sec	693	1653	1618	1655
	Water temperature oC	19.5	19.5	19.5	19.5
	Flow pressure kPa	335	335	335	335

ideal <+= 0.5 %	Variance to average	0.16%	-0.03%	-0.13%	Pass
	Actual flow rate ltr/hour	28.93	29.77	29.92	29.53
	Difference %	2.50%	2.79%	2.89%	2.76%
	Difference ltr	10.29	10.31	10.32	10.31
	End reading m3	16.31914	16.32945	16.33977	
30 l/h	Start reading m3	16.30885	16.31914	16.32945	
	Volume displacement ltr	10.029	10.030	10.030	10.030
	Test duration sec	1248	1213	1207	1223
	Water temperature oC	19.0	19.0	19.0	
	Flow pressure kPa	335	335	335	335

REMARKS:

Final signature test

Tested in series with 2 x 3 other meters of same type but different makes.

Water Meter - Test Report WRC Project Applicable Regulation Test type: Print date: 24 March 2000 SABS 1529-1 1994, section 6.4 and A 4.2h Customer: WRC Print time: 02:34:41 PM "3", Qp = 1.5 m3/h Manufacturer: Revised 16/06/99 Meter Size: -B-WRCsig-4.res File No.: Meter Class: Magnetic drive No Meter Type: Report No.: 3571/930507/R29 Route No: 3 Flow orientation: Test No: 992102 Receipt reading: P Group: Model: Working Pressure: Model AI 1 Meter Serial # Test#1 Test # 2 Test # 3 aver. 1-3 Test bench position 335 335 Flow pressure kPa Water temperature 18.5 18.5 18.5 18.5 σC 870 Test duration sec 868 Volume displacement 10.026 10.032 10.031 10.030 ltr 40 l/h Start reading 16.27826 16.28846 16.29867 m.3 16,29867 End reading m3 16.23846 16.30885 10.20 10.21 10.18 10.20 Difference ltr 41.51 1.74% Difference 1.49% 1.67% Actual flow rate 41.08 41.39 Variance to average ideal < -- 0.5 % 0.07% 0.11% 0.18% Pass Flow pressure 19.0 Water temperature 19.0 19.0 19.0 σC 732 Test duration 713 714 Sec 10.030 10.030 10.025 Volume displacement ltr 10.028 16.24796 16.25806 16 26816 50 l/h Start reading m3End reading m3 16.25806 16.26816 6.27826 Difference ltr 0.75% 0.71% 0.70% 0.70% Difference Actual flow rate lts/hour 49 11 50.64 50.55 50.16 ideal <-- 0.5 % Variance to average 0.02% 0.02% 0.03% Pass Flow pressure 19.5 Water temperature 19.5 19.5 19.5 of 497 497 491 495 Test duration sec 10.002 Volume displaceme 10.005 10.012 16.21783 16.21795 16.22795 16.23796 16.23796 16.24796 75 Vh Start reading m3 End reading m3 10.12 10.00 Difference 10.01 ltr 1.15% 0.37% Difference 0.02% 0.02% 2.47 Ite hour Actual flow rate ideal <-- 0.5 % Variance to average 0.78% 0.39% 0.39% Pass Flow pressure Water temperature 19.5 19.5 19.5 19.5 σC 336 369 365 Test duration 500 10.018 10.013 10.005 Volume displaceme 16.19778 16.20782 100 lh 16.18774 Start reading 16.20782 End reading m3 16.17778 16.21783 10.03 10.04 10.04 Difference ltr 0.27% 0.18%0.22% 0.05% Difference 107.28 98.68 Actual flow rate Variance to average ideal < -- 0.5 % 0.04% 0.09% 0.13% Pass Flow pressure 19.5 Water temperature οC 296 Test duration 289 Volume displacement 10.009 10.009 10.009 Itr 120 Vh 16.15758 16.16765 16.17769 16.17769 16.18774 Start reading m.3 16.16765 End reading m3 Difference 10.07 10.04 10.05 ltr 0.61% 0.31% 0.44% Difference 0.41% 121.87 Actual flow rate 124.68 120.51 120.51 ideal < -- 0.5 % Variance to average -0.17% 0.13% 0.03% Pass Test Place SABS Pretoria Test Date 28/05/99 E3 Date: Testing Officer Manager Date:

Signed

Signed

 Applicable Regulation
 Test type:
 WRC Project
 Print date:
 24 March 2000

 SABS 1529-1 1994, section 6.4 and A 4.2h
 Customer:
 WRC
 Print time:
 02:34:41 PM

 Meter Size:
 "3", Qp = 1.5 m3/h
 Manufacturer:
 Revised
 16:06:99

 Meter Class:
 "B"
 File No.:
 WRCsig-4.rex

 Meter Class:
 "B"
 File No.:
 WRCsig-4.res

 Magnetic drive
 No
 Meter Type:
 Report No.:
 3571/930507/R29

 Route No:
 3
 Flow orientation:
 Test No:
 992102

Receipt reading: P Group:

Model: Working Pressure:

lodet:	,	working Pressure:			
Meter Serial#	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1-3
Test bench position		# 3	# 3	# 3	
-	Flow pressure kPa	335	325	330	33
	Water temperature oC	20.0	19.5	20.0	19
	Test duration sec	186	185	179	18
	Volume displacement ltr	10.045	10.008	10.032	1
200 l/h	Start reading m3	16.12739	16 13747	16.14752	
	End reading m3	16.13747	16.14752	16.15758	
	Difference ltr	10.08	10.05	10.06	10.0
	Difference %	0.35%	0.42%	0.28%	0.35%
	Actual flow rate Itr/hour	194.42	194.75	201.76	196.93
ideal <+= 0.2 %	Variance to average	0.00%	-0.07%	0.07%	
	Flow pressure kPa	330	330	330	330

ideal <++ 0.2 %	Variance to average	-0.07%	0.08%	-0.02%	Pass
	Actual flow rate ltr/hour	496.50	503.65	503.65	501.25
	Difference %	1.61%	1.46%	1.56%	1.54%
	Difference ltr	10.23	10.22	10.23	10.2
	End reading m3	16.10694	16.11716	16.12739	
500 l/h	Start rending m3	16.09671	16.10694	16.11716	
	Volume displacement hr	10,068	10.073	10.073	10.07
	Test duration sec	73	72	72	7.
	Water temperature oC	20.0	19.5	19.5	19.
	Flow pressure kPa	330	330	330	33

ideal <+- 0.2 %	Variance to average	-0.21%	-0.18%	0.39%	Pass
	Actual flow rate ltr/hour	669.24	673.91	676.17	673.09
	Difference %	-0.91%	-0.04%	-0.61%	-0.22%
	Difference Itr	100.19	100.11	99.50	99.93
	End reading m3	15.89656	15.99667	16.09617	
675 Vh	Start reading m3	15.79637	15,89656	15.99667	
	Volume displacement ltr	100.200	100.150	100.110	100.153
	Test duration sec	539	535	533	536
	Water temperature oC	19.5	19.5	19.5	19.5
	Flow pressure kPa	320	3201	325	322

	Flow pressure kPa	320	320	320	320
	Water temperature oC	19.5	19.5	19.5	19.5
	Test duration sec	487	484	483	485
	Volume displacement ltr	100.340	100.170	100.160	100.223
750 l/h	Start reading m3	15.49645	15.59654	15.69644	
	End reading m3	15.59654	15.69644	15.79637	
	Difference ltr	100.09	99.90	99.93	99.97
	Difference %	-0.25%	-0.27%	-0.23%	-0.25%
	Actual flow rate ltr/hour	741.73	745.07	746.53	744.44
ideal <+- 0.2 %	Variance to average	-0.90%	0.02%	-0.02%	Pass

ideal <++ 0.2 %	Variance to average	0.97%	-0.06%	-0.02%	Pass
	Actual flow rate Itnhour	995,77	1012.65	992.73	1000.31
	Difference %	-0.40%	-0.27%	-0.31%	-0.33%
	Difference ltr	99.73	99.87	99.79	99.80
	End reading m3	15.29679	15.39666	15.49645	
1000 l/h	Start reading m3	15.19706	15.29679	15.39666	
	Volume displacement ltr	100,130	100.140	100.100	100.123
	Test duration sec	362	356	363	360
	Water temperature oC	18.0	19.0	19.5	18.8
	Flow pressure kPa	315	315	310	313

Differential flow ltr/h	500	750	1500	3000
Differential pressure kPa				
Manifold pressure kPa	ERR	ERR	ERR	ERR
Pressure test kPa				
Pressure test minutes		See final test sheet		

Water Meter - Te Applicable Regulation SABS 1529-1 1994, sec		Test type: Customer:	WRC Project	Print date: Print time:	24 March 2000 02:34:41 PM
deter Size:	"3", Qp = 1.5 m3/h	Manufacturer:		Revised	16.06.9
Meter Class:	"B"			File No.:	WRCsig-4.res
Magnetic drive	No	Meter Type:		Report No.:	3571/930507/R29
Route No:	3	Flow orientation:		Test No:	992102
Receipt reading:		P Group:			
Model:		Working Pressure:			
Meter Serial #	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1 -3
Test bench position		n 3	# 3	= 3	
	Flow pressure kPa	300	290	300	297
	Water temperature oC	21.0	230 0	21.0	90.7
	Test duration sec	245		241	240
	Volume displacement ltr		100.050	102.000	100.683
1500 l/h	Start reading m3	14.79366		14 99416	
	End reading m3	14.89396	14 99416	15,09677	
	Difference htr	100.30		102.61	101.04
	Difference %	0.30%	0.15%	0.60%	0.35%
ideal - 0.24	Actual flow rate Itr hour	1469.39		1523.65 0.25%	1508.16
ideal - +- 0.2 *o	Variance to average	0.7576	0.20%	0.2576	P.Res
	Flow pressure kPa	300	300	283	203
	Water temperature oC	19.5		22.0	
	Test duration sec	210		205	206
	Volume displacement ltr	100.200	100.140	100.030	100.123
1750 l/h	Start reading m3	14.39227	14,49272	14.59294	100.120
	End reading m3	14,49272	14.59294	14.69338	
	Difference Itr	100.45	100.22	100.44	100.37
	Difference %	0.25%	0.08%	0.41%	0.25%
	Actual flow rate ltr/bour	1717.71	1767.18	1756.62	1746.90
ideal < 0.2 %	Variance to average	-0./90%	0.17%	-0.16%	Pass
		The same of the sa	and the same of the same of	parent distance of these	
	Flow pressure kPa	945		9.40	942
	Water temperature oC	23.0		22.5	22.7
	Test duration sec	176	The second secon	178	177
2000 l/h	Volume displacement ltr Start reading m3	13.93012	100 230	100.240	100.217
2000 Un	The second secon	14,09071	14.09071	14.19131	
	End reading m3 Difference ltr	10.59		100.78	100 66
	Difference %	0.41%		0.54%	0.44%
	Actual flow rate Itr/hour			2027.33	2038 31
ideal < == 0.2 %	Variance to average	0.33%	0.07%	-0.10%	
	T AND INVESTIGATION OF THE PARTY OF THE PART	Name and Address of the Owner, where the owner, which is the owner, which is the owner, where the owner, which is the owner, where the owner, which is the owner, where the owner, which is the	The second second		-
	Flow pressure kPa	920	925	925	923
	Water temperature oC	22.5	23.0	23.0	22.8
	Test duration sec	144		144	144
	Volume displacement ltr	100.280	100.310	100.250	100.280
2500 l/h	Start reading m3	13.63727	13.78822	13.88921	
	End reading m3	13.78822	13.88921	13.99012	
	Difference ltr	100.95	100.99	100.91	100.95
	Difference "a	0.57%		0.66° is	0.67%
	Actual flow rate ltr/hour			2506.25	2507.00
ideal < == 0.2 %	Variance to average	-0.30%	-0.01%	0.01%	Pass
	-				
	Flow pressure kPa	920		900	913
	Water temperature oC	22.0		23.0	22.3
	Test duration see	132			132
2750 12	Volume displacement ltr			100.420	100.370
2750 l/h	Start reading m3	13.34363		13.58574	
-	End reading m3	13.43466		13.68727	101.21
	Difference hr Difference %	0.70%		101.53	0.84%
	Difference % Actual flow rate ltr.hour			2759.63	2737.36
	t change they take the front	47.0.47	8710.71	-0.27%	

Receipt reading: Model:	No. 3	Meter Type: Flow orientation:		Revised File No.: Report No.: Test No.	16-06-99 WRCsig-4-res 3571-930507-R29 992102
Allowhed:		P Group:			
Meter Serial #	Model AI 1	Working Pressure:	Test#2	Test #3	
Test bench position	Model Al 1	23	# 3	#3	aver. 1 -3
1 car senen position	Flow pressure kPa			890	887
	Water temperature oC	20.5	20.5	21.0	20.7
	Test duration sec	119	120	119	119
	Volume displacement It			100.480	100.470
3000 l/h	Start reading m3	13.07977		13.28232	
	End reading m3	13.13104		13.38363	
	Difference ltr	101.27		101.31	101.29
	Difference %	the second secon	The second secon	0.83%	0.81%
	Actual flow rate Itr hou			3039.73	3030.94
ideal <++ 0.2 %	Variance to average	0.91%	0.01%	-0.01%	Pass
	Flore services		TOTAL PROPERTY.		-
	Flow pressure kPa	890 20.5		880	887
	Water temperature oC Test duration sec	20.5	110	19.5	19.7
	Volume displacement Its		100.520	100.530	100 517
3250 L/h	Start reading m3	12,77574	12.87709	12.97842	100.31
3230 EH	End reading m3	12.87709		13.07977	
	Difference ltr	101.35		101.35	101.34
	Difference %		0.81%	0.82%	0.82%
	Actual flow rate Itr hou			3290 07	3279.70
ideal <+- 0.2 %	Variance to average	-0.32%	0.02%	0.01%	
	Water temperature oC Test duration see Volume displacement lit Start reading m3 End reading m3 Difference lit Difference lit Actual flow rate lit hou Variance to average Flow pressure kPa Water temperature oC Test duration see Volume displacement lite				
	Start reading m3				
	End reading m3				
	Difference ltr				
	Difference %				
	Actual flow rate Itr hour				
	Variance to average				
	Flow pressure kPa				
	Water temperature oC				
	Test duration sec				
	Volume displacement ltr				
	Start reading m3				
	End reading m3				
	Difference ltr				
	Difference %				
ideal < +- 0.2 %	Actual flow rate Itr hour Variance to average				

REMARKS:

Water Meter - Test Report

Final signature test Tested in series with 2 x 3 other meters of same type but different makes.

Water Meter - T Applicable Regulation		Test type:	WRC Project	Print date:	24 March 2000
SABS 1529-1 1994, secti	on 6.4 and A.4.2h	Customer:	WRC	Print time:	02:43:32 PM
Meter Size:	"3", Qp = 1,5 m3/h	Manufacturer:		Revised	15/06/99
Meter Class:	-B-			File No.:	WRC22.5 res
Magnetic drive	No	Meter Type:		Report No.:	3571/930507/R29
Route No:	3	Flow orientation:		Test No.	9828-02
Receipt reading:		P Group:			
Model:		Working Pressure:			
Meter Scripl #	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1-3
Test bench position	Model Al 1	# 3	13	13	Iver. 1 -3
1 est benen pestison	Flow pressure kPa			310	310
TEST FLOW RATES	Water temperature oC	20.5		20.5	20.5
LEST PLOT BOLLES	Test duration ses		1176	1180	1183
	Volume displacement It			10.030	10.030
.В.	Start reading m3			9.14094	10.000
30 ltr/h	End reading m3		9.14094	9.15126	
30 10.0	Difference la			10.32	10.34
		6 3.49%		2.89%	3.12%
	Actual flow rate Its hos		A commence of the company of the com	30.60	30.54
ideal < 0.5 %	Variance to average	-0.37%		0.23%	
100.00	variance to average	10.57.76	0.14-0	0.25 76	1.833
	Flow pressure kPa	320	320	320	35
	Water temperature of		Annual Control of the	21.0	
	Test duration sec			278	282
	Volume displacement It			9 997	9 996
-B-	Start reading m3			9.18138	7.777
120 ltr/h	End reading m3	The same of the sa	4	9.19139	
120 0010	Difference ltr			10.01	10.04
		6 0.81%		0.13%	0.38%
	Actual flow rate linhor	the state of the s		129.46	127.49
ideal <++ 0.5 %	Variance to average	-0.43%		0.25%	
Indian Control of	Tarrance to average	19.40 10		0.22.0	1 444
of Street, out of Street, or other	Flow pressure kPa	320	3201	320	3.70
0.5 Qp	Water temperature oC			19.0	
	Test duration sec			534	
	Volume displacement It	the state of the s	A	100.200	100.163
"A" to "D"	Start reading m3			9.39178	1.00.100
750 ltr/hour	End reading m3	The second secon	A CONTRACTOR OF THE PARTY OF TH	9,49205	
720 111111111	Difference Its			100 27	100.22
		16 0.07%		0.07%	0.06%
	Actual flow rate Itr/hos		4	675.51	680.78
ideal <++ 0.2 %	Variance to average	-0.01%		-0.01%	AND RESIDENCE OF THE PARTY OF T
100.00	Tallance to average	-0.0174			1 100
Contraction of the second	Flow pressure kPs	300	300	\$50	100
1.00 Op	Water temperature of			19.0	19.6
1.00 529	Test duration sec			227	233
	Volume displacement 1			100.100	100.117
"A" to "D"	Start reading ma3		the same of the sa	9.69211	100.11
1500 ltr/hour	End reading m3			9.79233	
Econ strainer	Difference Its	and the second s	A	100.22	100.05
		% -0.16%		0.12%	
	Actual flow rate Ite hos			1587.49	
ideal 0.2 %	Variance to average	0.14%		-0.14%	
PICE TO S	variance to average	0.14	0.01.0		1 444
	Flow pressure kP	915	9151	915	913
1.00 Qs	Flow pressure kP: Water temperature of			18.5	
1.00 (3	Test duration sec			120	119
		tr 100.350		100.360	
"A" to "D"	Start reading m3			10.10717	
3000 ltr/hour	End reading m3			10.20841	
2000 All Hotel				101.24	100.94
		% 0.43%		0.88%	0.49%
					Andread Control of the Control of th
	Actual flow rate http://	ur 3035.80	3035.19	3010.80	3027.22

REMARKS

Box configureation with ball valve upstream from meter. Valve opening "22.5 degree CPEN". Meter in series with two others of same make. Tested at 5 flows to SABS 1529-1 and two others as per selection of SIGNATURE GRAPH.

FLOW RATE Water temperature oC 21.5 21.5 354 (Meter curve) Test duration sec 362 354 Volume displacement ltr 10.013 10.013 10.013 10.15 100 lu/hear Start reading m3 10.42416 10.44421 10.45 End reading m3 10.44421 10.45424 10.46 Difference ltr 10.05 10.03 10 Difference % 0.37% 0.17% 0.37 Actual flow rate ltr/hour 99.58 101.83 101 Variance to average 40.09% 0.11% 4.06 Flow pressure kPa 335 335 FLOW RATE Water temperature oC 21.5 21.5 2.0 (Meter curve) Test duration sec 73 71 Volume displacement ltr 10.047 10.048 10.0 Start reading m3 10.46428 10.47456 10.48475 10.494 Dufference ltr 10.28 10.19 10.494 Dufference ltr 10.28 10.19 10.996 Dufference % 2.32% 1.41% 1.596 Actual flow rate ltr/hour 495.47 509.48 509		rch 200
Meter Type: File No. Meter Type: Report No. Report No. Soute No.		3:32 P3
Magnetic derive No		15/06/9
Courte No. Company Courte No.		C22.5.re
Note		9828-0
Meter Serial # Model AI Test #1 Test #2 Test #3		2020 0
FLOW RATE		
FLOW RATE	13 aver. 1	1.3
FLOW RATE Waise temperature OC 21.5	aver. I	1-3
Motor curve Test duration Sec 362 534	300	32
Volume displacement Ir 10 013 10.013 10.015 Indirection Ir 10.43416 10.44421 10.45 End reading m3 10.44421 10.45424 10.45 End reading m3 10.44421 10.45424 10.45 Difference Ir 10.05 10.03 16 Difference 56 0.3756 0.1796 0.1796 0.19 Actual flow rate Itr-hour 99.58 101.83 101 Variance to average 0.6996 0.1168 0.85 Flow pressure KPa 335 335 335 FLOW RATE Water temperature oC 21.5 22.5 22.5 C(Meter curve) Test duration see 73 71 Volume displacement Ir 10.047 10.048 10.045 S00 le/hour Start reading m3 10.45428 10.47456 10.4847 End reading m3 10.45428 10.47456 10.484 Difference Itr 10.28 10.19 10 Difference Itr 10.28 10.19 10 Difference 0.5796 0.3395 0.30 Variance to average 0.4.7796 0.3395 0.30 Flow pressure KPa Water temperature oC Test duration see volume displacement Itr Start reading m3 Difference 10 0.4796 0.3395 0.30 Flow pressure KPa Water temperature oC Test duration see volume displacement Itr Start reading m3 Difference 10 0.4796 0.3395 0.30 Flow pressure KPa Water temperature oC Test duration see volume displacement Itr Start reading m3 Difference 10 0.4796 0.3395 0.30 Flow pressure KPa Water temperature oC Test duration see volume displacement Itr Start reading m3 Difference 10 0.4796 0.30 0.30 Flow pressure KPa Water temperature oC Test duration see volume displacement Itr Start reading m3 Difference 10 0.4796 0.30 0.30 Flow pressure KPa Water temperature oC Test duration see volume displacement Itr Start reading m3 Difference 10 0.4796 0.30 0.30 Flow pressure KPa Water temperature oC Test duration see 0.4796 0.30 0.30 0.30 Flow pressure KPa Water temperature oC 0.30 0.30 0.30	21.5	21
100 lt/hour	356	35
End reading m3	10.010	10.01
Difference 1tr 10.05 10.03 15 Difference 5% 0.375% 0.175% 0.15 Actual flow rata 1tr hour 99.58 101.83 101 Variance to average 0.095% 0.11% 0.88 Flow pressure KPa 335 335 Flow pressure KPa 335 335 FLOW RATE Water temperature o.C. 21.5 21.5 22.5 (Meter curve) Test duration nec 73 71 Volume displacement tr 10.047 10.048 10.0 Start reading m3 10.47456 10.4847 10.484 End reading m3 10.47456 10.4847 10.48 End reading m3 10.47456 10.4847 10.49 Difference % 2.325% 1.41% 1.54 Actual flow rate Itr-hour 495.47 509.48 500 Variance to average 0.4775% 0.33% 0.24 Flow pressure KPa Water temperature o.C. Test duration no no no no Full reading m3 Difference tr Difference tr Start reading m3 Difference tr Difference tr Difference tr Start reading m3 Difference tr Difference tr Difference tr Difference tr Difference tr Difference tr Start reading m3 Difference tr Start reading m3 Difference tr Difference tr Difference tr Start reading m3 End reading m3 End reading m3 Difference tr Start reading		
Difference	10.04	10.0
Actual flow rate Itr hour 99.58 101.82 101	0.30%	0.285
Flow pressure KPa 335 2.35	101.22	100.8
FLOW RATE Water temperature oC 21.5 21.5 21.5 (Meter curva) Test duration see 73 71 10.48 10.047 10.048 10.045 10.047 10.048 10.047 10.048 10.047 10.048 10.047 10.048 10.047 10.048 10.047 10.048 10.048 10.047 10.048 10.047 10.048 10.048 10.047 10.048	-0.02% Pass	
FLOW RATE Water temperature oC 21.5 21.5 21.5 (Meter curve) Test duration see 73 71 71 Volume displacement hr 10.047 10.048 10.04 500 hr/hour Start reading m3 10.44.25 10.474.56 10.48 10.04 End reading m3 10.44.25 10.474.55 10.48 10.04 End reading m3 10.44.25 10.474.55 10.48 10.04 End reading m3 10.474.56 10.484.75 10.49 10.00 End reading m3 10.474.56 10.484.75 10.49 10.00 End reading m4 m4 m4 m4 m4 m4 m4 m		
Meter curve Test duration sec 73 71	335	33
Volume displacement tr 10.047 10.048 10.4	21.5	21.
Sizet reading m3	10.039	10.04
End rending m3	.48475	10.04
Difference 1tr 10.28 10.19 10 Difference 96 2.23% 1.41% 1.59 Astual flow rate Itrhour 495.47 509.48 509 Variance to average 4.57% 6.33% 6.24 Flow pressure kPa	.49494	
Actual flow rate Itehour 495.47 509.48 509	10.19	10.2
Variance to average -0.57% 0.33% 0.24	1.50%	1.759
Flow pressure kPs Water temperature oC Test duration see Volume displacement ltr Start reading m3 End reading m3 Difference 96 Actual flow rate ltr/hour Variance to average Flow pressure kPs Water temperature oC Test duration see Volume displacement ltr Start reading m3 End reading m3 Difference ltr Difference ltr Difference ltr Difference ltr Difference 96 Actual flow rate ltr/hour Variance to average Flow pressure kPs Water temperature oC Test duration see Volume displacement ltr Start reading m3 End reading m3 Difference ltr Difference 96 Actual flow rate ltr/hour Variance to average Flow pressure kPs Water temperature oC Test duration see Volume displacement ltr Start reading m3 End reading m3 Difference ltr Difference ltr Start reading m3 End reading m3 End reading m3 End reading m3 Difference ltr Difference 165 Actual flow rate ltr/hour Variance to average	509.02	504.5
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Difference % Actual flow rate ltr/bour Variance to average st Place SABS Pretoria		
Actual flow rate ltr/hour Variance to average SABS Pretoria		
Variance to average est Place SABS Pretoria		
st Date 09/07/98		
sting Officer Date:/_/ Manager Date:/_/	,	
sting Officer Date:// Manager Date://		

water wieter - 1	est Report				
Applicable Regulation		Test type:	WRC Project	Print date:	28 March 2000
SABS 1529-1 1994, sect		Customer:	WRC	Print time:	09:47:35 AM
Meter Size:	"3", Qp = 1,5 m3/h	Manufacturer:		Revised	15/06/99
Meter Class:	"B"			File No.:	wretst-1.rex
Magnetic drive	No	Meter Type:		Report No.:	3571/930507/R29
Route No:	3	Flow orientation:		Test No:	9827-01
Receipt reading:	6.23739	P Group:			
Model:		Working Pressure:			
Meter Serial #	Model AI 1	Test # 1	Test # 2	Test#3	aver. 1 -3
Test bench position	Prince Par a	#1	# 1	#1	200.1.0
110000000	Flow pressure kPa	335		335	335
TEST FLOW RATES	Water temperature oC	19.5	A CONTRACTOR OF THE PARTY OF TH	19.5	19.5
	Test duration sec	1157		1176	1169
	Volume displacement htr	10.030		10.027	10.025
.B.	Start reading m3	6.43867		6.45921	10.040
30 ltr/h	End reading m3	6.44895		6.46950	
JU 111 11	Difference ltr	10.28	A THE RESIDENCE OF THE PARTY OF	10.29	10.28
	Difference %	2.49%		2.62%	2.51%
-	Actual flow rate Itr/hour	31.21		30.69	30.87
ideal <+- 0.5 %	Variance to average	0.01%	and the second s	-0.12% P	
10cal < 74 0.5 %	variance to average	0.0110	0.10:0	-0.12~e F	455
	Flow pressure kPa	335	335	335	335
	Water temperature oC	19.5	19.5	19.5	19.5
	Test duration sec	284	282	283	283
	Volume displacement ltr	9.997	9.999	9.999	9,998
"B"	Start reading m3	6.47027		6.50021	
120 ltr/h	End reading m3	6.48023		6.51016	
100 100 100	Difference ltr	9.96		9.05	9.95
	Difference %	-0.37%	-0.49%	-0.49%	-0.45%
	Actual flow rate ltr hour	126.72	A manufacture of the state of t	127.20	127.19
ideal <+= 0.5 %	Variance to average	-0.08%		0.04% P	
THE RESERVE TO STATE OF THE PARTY OF THE PAR		THE PERSON NAMED IN COLUMN	monagement or manufacture for	The second second	STATE OF THE PARTY
	Flow pressure kPa	325	330	330	328
0.5 Qp	Water temperature oC	17.0	17.5	19.5	18.0
	Test duration sec	524	520	525	523
	Volume displacement ltr	100.230	100.150	100.290	100.223
"A" to "D"	Start reading m3	6.51016	6.61065	6.71103	
750 ltr/hour	End reading m3	6,61065	6.71103	6.81154	
	Difference ltr	100.49	100.38	100.51	100.46
	Difference %	0.26%	0.23%	0.22%	0.24%
	Actual flow rate ltr/hour	688.60	693.35	687.70	689.87
ideal <++ 0.2 %	Variance to average	-0.02%	0.01%	0.02% P	ass
	Flow pressure kPa	310		310	310
1.00 Qp	Water temperature oC	19.0		19.0	19.0
	Test duration sec	250	250	251	250
	Volume displacement Itr	100.140	100.140	100,090	100.123
"A" to "D"	Start reading m3	6.81154	6.91169	7.01182	
1500 itn/hour	End reading m.3	6.91169	7.01182	7.11190	
	Difference ltr	100.15	100.13	100.08	100.12
	Difference %	0.01%	-0.01%	-0.01%	-0.00%
	Actual flow rate Itr/hour	1442.02	1442.02	1435.55	1439 86
ideal < == 0.2 %	Variance to average	-0.01%	0.01%	0.01°6 P	ass
Contracting the West and Street					
	Flow pressure kPa	820		820	820
1.00 Qs	Water temperature oC	19.5		19.5	19.5
	Test duration sec	126		125	125
	Volume displacement ltr	100.420		100.380	100.400
"A" to "D"	Start reading m3	7.11206		7.31416	
3000 ltr:hour	End reading m3	7.21311		7.41516	
	Difference ltr	101.05		101.00	101.03
	Difference %	0.63%		0.62%	0.63%
	Actual flow rate ltr-hour	2869.14		2890.94	2883.83
ideal ≤++ 0.2 %	Variance to average	0.00%	-0.02%	0.01% P	ass

REMARKS

Water Meter - Test Report

Box configureation with ball valve upstream from meter. Valve opening "FJLL OPEN" Meter in series with two others of same make. Tested at 5 flows to SABS 1529-1 and two others as per selection of SIGNATURE GRAPH.

Water Meter - Tes Applicable Regulation (ABS 1529-1 1994, sec Meter Size: Meter Class: Magnetic drive Route No: Receipt reading: Model:		Test type: Customer: Manufacturer: Meter Type: Flow orientation: P Group: Working Pressure:	WRC Project WRC	Print date: Print time: Revised File No.: Report No.: Test No:	28 March 2000 09:52:07 AM 15:06:99 wretst-Lres 3571/930507/R29 9827-01
Meter Serial #	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1 -3
Test bench position	1.33441.34	8 1	# 1	E	
Test oction position	Flow pressure kPa	325	325	325	325
FLOW RATE	Water temperature oC	19.5	19.5	19.5	
(Meter curve)	Test duration sec	357	358	358	
	Volume displacement ltr	10.020	10.015	10.020	10 018
100 lt/hour	Start reading m3	9.05873	9.06873	9.07873	
	End reading m3	9.06873	9.07873	9.08874	
	Difference ltr	10.00	10.00	10.01	10.00
	Difference %	-0.20%	-0.15% 100.71	-0.10%	
	Actual flow rate ltr/hour Variance to average	101.04	0.00%	100.76 -0.05%	
A CONTRACTOR OF THE PARTY OF TH	variance to average	0.0376	0.0076	-0.0574	Fass
THE RESERVE OF THE PARTY OF	Flow pressure kPa	330	330	330	330
FLOW RATE	Water temperature oC	20.0	20.0	20.0	20.0
(Meter curve)	Test duration sec	72	72	72	72
	Volume displacement ltr	10.049	10.043	10.043	10.045
500 lt/hour	Start reading m3	9.08874	9.09894	9.10915	
	End reading m3	9.09894	9.10915	9.11938	
	Difference Itr	10.20	10.21	10.23	10.21
	Difference %	1.50%	1.66%	1.86%	
	Actual flow rate ltr:hour	502.45	502.15	502.15 -0.19%	502.25
	Variance to average	0.1776	0.01%	-0.19%	Fass
According to the Control of the Cont	Flow pressure kPa	1		-	The second secon
	Water temperature oC				
	Test duration sec				
	Volume displacement ltr				
	Start reading m3				
	End reading m3				
	Difference ltr				
	Difference %				
	Actual flow rate htt/hour				
	Variance to average		-		-
AND THE PERSON NAMED IN	Flow pressure kPa			-	-
	Water temperature oC Test duration sec				
	Volume displacement Itr				
	Start reading m3				
	End reading m3				
	Difference ltr				
	Difference %				
	Actual flow rate Itr hour				
	Variance to average				
	Flow pressure kPa				
	Water temperature oC				
	Test duration sec				
	Volume displacement ltr				
	Start reading m3				
	End reading m3				
	Difference hr Difference %				
	Actual flow rate ltr hour				
	PROBLEM SHEET STORY	-			

	Actual flow rate ltnhour Variance to average			
Test Place Test Date	SABS Pretoria 02/07/98			
Testing Officer	Date:/	Manager	Date://	
	Signed		Signed	E16

Water	Meter -	Test	Report

Applicable Regulation	om.	Test type:	WRC Project	Print date:	24 March 2000
SABS 1529-1 1994,	section 6.4 and A 4.2h	Customer:	WRC	Print time:	02:45:49 PM
Meter Size:	"3", Qp = 1,5 m3/h	Manufacturer:		Revised	16/06/99
Meter Class:	"B"			File No.:	WRC45T.rex
Magnetic drive	No	Meter Type:		Report No.:	5421/930507/R29
Route No:	3	Flow orientation:		Test No:	991901
Receipt reading:		P Group:			

Model: Working Presoure:

Meter Serial #	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1 -3
Test bench position		# 3	#3	#3	-
	Flow pressure kPa	335	335	335	335
TEST FLOW RATES	Water temperature oC	21.0	21.0	21.0	21.0
	Test duration sec	1134	1108	1110	1117
	Volume displacement ltr	1-3.022	10.035	10.024	10.027
"B"	Start reading m3	11.61038	11.61927	11.62811	
30 ltr/h	End reading m3	11.61927	11.62811	11.63698	
	Difference ltr	8.89	8.84	8.87	8.87
	Difference %	-11.30%	-11.91%	-11.51%	-11.57%
	Actual flow rate Itr/hour	31.82	32.60	32.51	32.31
ideal < == 0.5 %	Variance to average	-0.28%	0.34%	-0.06%	
					AND DESCRIPTION OF THE PARTY OF
	Flow pressure kPa	325	325	325	325
	Water temperature oC	21.0	21.0	21.0	21.0
	Test duration sec	286	277	277	280
	Volume displacement ltr	10.009	10.011	10.011	10.010
"B"	Start reading m3	11.55077	11.56075	11.57072	
120 ltr/h	End reading m3	11.56075	11.57072	11.58070	
	Difference ltr	9.98	9.97	9.98	9.99
	Difference %	-0.29%	-0.41%	-0.31%	-0.34%
	Actual flow rate ltr/hour	125.99	130.11	130.11	128 70
ideal <++ 0.5 %	Variance to average	-0.05%	0.07%	-0.03%	
		THE RESERVE OF THE PARTY OF THE	The second secon	THE R. P. LEWIS CO., LANSING, MICH.	Company of the Compan
	Flow pressure kPa	320	320	320	3.20
0.5 Qp	Water temperature oC	20.5	20.5	20.5	20.5
	Test duration sec	483	485	485	484
	Volume displacement ltr	100,160	100.240	100.200	100.200
"A" to "D"	Start reading m3	11.20457	11.30454	11.40457	
750 ltr/hour	End reading m3	11.20454	11.40457	11.50458	
	Difference ltr	99.97	100.03	100.01	100.00
	Difference %	-0.19%	-0.21%	-0.19%	-0.20%
	Actual flow rate ltr/hour	746.53	744.05	743.75	744.78
ideal <++ 0.2 %	Variance to average	-0.01%	0.01%	-0.01%	Pass
the plants of the later of		The state of the s		THE RESERVE TO STREET,	hep-first balleton of Fig. 11
	Flow pressure kPa	310	310	310	310
1.00 Qp	Water temperature oC	20.0	20.0	20.0	20.0
	Test duration sec	249	248	2,50	249
	Volume displacement ltr	10).090	100.140	100 180	100.137
"A" to "D"	Start reading m3	10.90390	11.00414	11.10436	
1500 ltr/hour	End reading m3	11.00414	11.10436	11.20457	
	Difference ltr	100.24	100.22	100 21	100.22
	Difference %	0.15%	0.08%	0.03%	0.09%
	Actual flow rate Itr hour	1447.08	1453.65	1442.59	1447.76
17.7	11 1	0.000	0.0101	B (CCB)	

	Actual flow rate - its nour	1447.08	1423.63	1442.39	1447.70
ideal < 0.2 %	Variance to average	-0.06%	0.01%	0.06%	Pass
	The second secon	8101	0177		
	Flow pressure kPa	910	915	915	913
1.00 Qs	Water temperature oC	19.5	19.5	19.5	19.5
	Test duration sec	118	119	119	119
	Volume displacement ltr	10/0.450	100.450	100.440	100.447
"A" to "D"	Start reading m3	10.60009	10.70138	10.80268	
3000 ltr/hour	End reading m3	10.70138	10.80268	10.90390	
	Difference ltr	131.29	101.30	101.22	101.27
	Difference %	0.84%	0.85%	0.78%	0.82%
	Actual flow rate lig/hour	30-54.58	3038.82	3038.52	3047.26
ideal <++ 0.2 %	Variance to average	-0.02%	-0.03%	0.04%	Pass

REMARKS

Normal manifold installation with meter rotated 45 degrees from the vertical.

Tested at 5 flows to SABS 1529-1 and two others as per selection of SIGNATURE GRAPH.

Water Meter - Tes Applicable Regulation SABS 1529-1 1994, sec	tion 6.4 and A 4.2h	Test type: Customer:	WRC Project WRC	Print date: Print time:	24 March 200 02:45:49 PS
Meter Size: Meter Class:	"3", Qp = 1,5 m3/h	Manufacturer:		Revised File No.:	16/06/9 WRC45T.re
Magnetic drive	No	Meter Type:		Report No.:	5421/930507/R2
Route No:	3	Flow orientation:		Test No:	99190
Receipt reading:		P Group:			
Model:		Working Pressure:			
Meter Serial # Test bench position	Model AI 1	Test # 1	Test #2	Test #3	aver. 1 -3
rescuence position	Flow pressure kPa	325		325	32:
FLOW RATE	Water temperature oC	21.5		21.5	21.
(Meter curve)	Test duration sec	364	362	362	
	Volume displacement ltr	10.014	10.014	10.014	10.01
100 itr/hour	Start reading m3	11.58070	11.59060	11 60049	
	End reading m3	11.59060		11.61038	
	Difference Itr	9.90		9 89	
	Difference %	-1.14%			
	Actual flow rate Itrhour Variance to average	99.04			
	variance to average	-0.0776	0.00 %	0.05%	L 244
	Flow pressure kPa	3.20	320	320	32
FLOW RATE	Water temperature oC	20.5		20.5	20.:
(Meter curve)	Test duration sec	73	73		7.
	Volume displacement ltr	10.074	10.064	10.066	10.06
500 ltr/hour	Start reading m3	11.52020	11.53041	11.54060	
	End reading m3	11.53041	11.54060	11.55077	
	Difference Itr	10.21		10.17	
	Difference %	1.35%	1.25%	1.03%	1.219
	Actual flow rate Itr/hour	496.40	496.31	496.41	496.5
A COMPANY OF THE PARTY OF THE P	Variance to average	-0.14%	-0.0476	0.18%	P 355
	Flow pressure kPa	-		-	
	Water temperature oC				
	Test duration sec				
	Volume displacement ltr				
	Start reading m3				
	End reading m3				
	Difference ftr				
	Difference %				
	Actual flow rate lite hour				
Chicago Company	Variance to average	CONTRACTOR OF STREET	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN 2 IN COLUMN	married Married States	
I STATE OF THE STA	Flow pressure kPa				
	Water temperature oC				
	Test duration sec				
	Volume displacement ltr			,	
	Start reading m3				
	End reading m3				
	Difference ltr				
	Difference % Actual flow rate ltmhour				
	Actual flow rate Itr/hour Variance to average				
	- variance to average	Name and Address of the Owner, where	The second secon	And the second second second	
	Flow pressure kPa		-		
	Water temperature oC				
	Test duration sec				
	Volume displacement ltr				
	Start reading m.3				
	End reading m3				
	Difference [tr				
	Difference %				
	Actual flow rate Ite hour				
	Variance to average	-			-
est Place est Date	SABS Pretoria 15/05/99				
Costing Officer	Date://_		Manager	Date://_	
	Signed			Signed	E
ABS Water meter laborre	story (012) 428-7089			WRC45T.rex	Page 2 of 2

Applicable Regulation SABS 1529-1 1994, sect Meter Size:	tion 6.4 and A 4.2h "3", Qp = 1,5 m3/h "B"	Test type: Customer : Manufacturer:	WRC Project WRC	Print date: Print time: Revised	24 March 2000 02:50:28 PM 15:06:99
Meter Class: Magnetic drive	No	Meter Type:		File No.: Report No.:	WRC45.res 3571/930507/R29
Route No:	3	Flow orientation:		Test No:	9827-01
Receipt reading:	6.23739	P Group:		1011.10	30701
Model:	0.23 37	Working Pressure	1		
Meter Serial #	Model AI 1	Test#1	Test#2	Test #3	aver. 1-3
Test bench position		#3	#3	#3	
	Flow pressure	Ps 3.	330	330	330
TEST FLOW RATES	Water temperature	oC 21	0 20.5	20.0	20.5
		sec [1		1145	1151
	Volume displacement	ltr 10.00	20 10.030	10.032	10.027
"B"		n3 7.734		7 8 562	
30 ltr/h		n3 7.835		7 82588	
	Difference	tr 10		10.26	10.35
	Difference	% 3.294	3.99%	2.27%	3.18%
	Actual flow rate lts/	hour 30.1		31.54	31.35
ideal <+- 0.5%	Variance to average	-0.11	-0.80%	0.91%	Pass
	T-1		100	700	
			35 330 200	330	330
				20.0	
			M 301	302	301
45.4	Volume displacement	ltr 6.9		9 995	9 994
,B,		nJ 7.815		7.85582	
120 Nr/h		n3 7.845	80 7.85582	7.86588	
	Difference	ltr 100		10.06	10 05
	Difference	% 0.76*		9.65%	0.56%
		bour 119		119 15	119 40
ideal <+- 0.5 %	Variance to average	-0.204	0.29%	-0.09%	Pass
-		The same of	277	777	-
0.7.0-		(Pa 3	15 17.5	17.5	17.5
0.5 Qp					
		500 5		535	533
111111111111111111111111111111111111111	Volume displacement	ltr 100.20		100 200	100 183
"A" to "D"		n3 7.8-i5		8.06599	
750 Itr/hour		n3 7.969		3.16602	
	Difference	ltr 1000		100.03	100.05
	Difference	% -0.14*		-0.17%	-0.14%
ideal or Addi		brug 661.		674.24	677.08
ideal <+- 0.2 %	Variance to average	0.00	-0.04%	0.03%	Pass
-	Flow pressure	cPa 3	330	330	332
1.00 Qp			0 18.5	18.5	18.7
			33 254	254	254
	Volume displacement	ltr 100 H		100 140	100 130
"A" to "D"		n3 8.1-66		8.36571	
1500 Itr/hour		n3 82/5		8 46550	
	Difference	ltr 991		99.79	99.81
	Difference	5% -0.72*		-0.35%	-0.30%
		hour 1424.		1419 31	1421.03
ideal <=- 0.2%	Variance to average	-0.18		0.05%	
	Taranta to arriva				
Married Street, Square, or other party of the last of	Flow pressure	Pa 9	0 915	913	913
1.00 Qs		aC 19	5 19.5	19.5	19.5
			18 119	119	119
	Volume displacement	itr 100.4		100.430	100 427
"A" to "D"		m3 8 5 5 7		\$ 75896	
	End reading :	n3 8 6 18.		8.85971	
				100.75	100.76
3000 Ite/hour		ltr 1001	81 100 73	100.75	1100 (10)
	Difference	No 100		0.32%	
	Difference Difference	hour 30e4	6.33%	0.32% 3038 22	0.34% 3046.65

REMARKS

Water Meter - Test Report

Box configureation with ball valve upstream from meter. Valve opining "45 degree OPEN" Meter in series with two others of same make. Tested at 5 flows to SABS 1529-1 and two others as per selection of SIGNATURE GRAPH.

Water Meter - Test Applicable Regulation SABS 1529-1 1994, sec Meter Size: Meter Class: Magnetic drive Route No: Receipt reading: Model:		Test type: Customer: Manufacturer: Meter Type: Flow orientation: P Group: Working Pressure:	WRC Project WRC	Print date: Print time: Revised File No.: Report No.: Test No:	24 March 2000 02:50:28 PM 15/06/99 WRC45.rex 3571/930507/R29 9827-01
Meter Serial #	Model AI 1	Test # 1	Test # 2	Test #3	aver. 1 -3
Test bench position	Flow pressure kPa	335	# 3	# 3	335
FLOW RATE	Water temperature oC	19.5	19.5		
(Meter curve)	Test duration sec	359	Annual Control of the		
	Volume displacement ltr	10.013	10.019	10.015	
100 ltr/hour	Start reading m3	8.46799		2172777	
	End reading m3	8.47799	8.48799	the state of the s	
	Difference ltr Difference %	-0.13%	-0.19%		10.00
	Actual flow rate Itn'hour	100.41	100.47	100.43	
	Variance to average	-0.06%	-0.00%		
	Flow pressure kPa	335	335	335	335
FLOW RATE	Water temperature oC	19.5	19.5	19.5	
(Meter curve)	Test duration sec	71	72	72	
foo bedown	Volume displacement ltr Start reading m3	10.040 8.49798	10.040 8.50714	10.045 8.51729	10.042
500 ltr/hour	Start reading m3 End reading m3	8.50714	8.51729	8.52748	
	Difference Its	9.16	10.15	10.19	9.83
	Difference %		1.10%	1.44%	-2.07%
	Actual flow rate Itr/hour	509.07	502.00		504.42
	Variance to average	6.69%	-3.17%	-3.52%	Pass
-	170	-		_	-
	Flow pressure kPa Water temperature oC				
	Test duration sec				
	Volume displacement ltr				
	Start reading m3				
	End reading m3				
	Difference ltr				
	Difference %				
	Actual flow rate Itr/hour Variance to average				
	variance to average	THE RESERVE OF THE PERSON NAMED IN			
	Flow pressure kPa				
	Water temperature oC				
	Test duration sec				
	Volume displacement ltr				
	Start reading m3 End reading m3				
	Difference ltr				
	Difference %				
	Actual flow rate ltr/hour				
	Variance to average				
	Flow pressure kPa				
	Water temperature oC Test duration sec				
	Volume displacement ltr				
	Start reading m3				
	End reading m3				
	Difference Itr				
	Difference %				
	Actual flow rate Itr/hour				
Test Place	Variance to average SABS Pretoria				
Tost Date	03/07/98				
Testing Officer	Date://		Manager	Date://	
	Signed			Signed	
SABS Water meter labora	tory (012) 428-7089			WRC45 rex	E14

Water Meter - Test Repor	Water	Meter -	Test	Repor
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Applicable Regulation	on	Test type:	WRC Project	Print date:	24 March 2000
SABS 1529-1 1994,	section 6.4 and A 4.2h	Customer:	WRC	Print time:	02:23:23 PM
Meter Size:	"3", Qp = 1,5 m3/h	Manufacturer:		Revised	16/06/99
Meter Class:	"B"			File No.:	WRCfit.rex
Magnetic drive	No	Meter Type:		Report No.:	5421/930507/R29
Route No:	3	Flow orientation:		Test No:	991901
Receipt reading:		P Group:			
** * * *		Washing Bearings			

Receipt reading: Model:		Group: Vorking Pressure:			
Meter Serial #	Model AI 1	Test # 1	Test # 2	Test#3	aver. 1 -3
Test bench position	Modelita	N 3	N 3	#3	2161.10
test bench position	Flow pressure kPa	335	335	335	33
EST FLOW RATES	Water temperature oC	19.5	19.5	19.5	19.
EST PLOW BATES	Test duration sec	1117	1117	1119	
	Volume displacement ltr	10.024	10.019	10.039	10.02
"B"	Start reading m3	12,70319	12.71353	12.72385	10.02
30 ltr/h	End reading m3	12.71353	12.72385	12.73416	
30 10111	Difference ltr	10.34	10.32	10.31	10.3
	Difference %	3.15%	3.00%	2.70%	2.959
	- Contraction -	32.31	32.29	32.30	
Mark Co. O. Co.		-0.20%	-0.05%	0.25% F	32.3
ideal < == 0.5 %	Variance to average	-0.20%	-0.0576	0.25% F	all
	Flow pressure kPa	320	3201	320	32
	Water temperature oC	19.5	19.5	19.5	19
	Test duration sec	280	281	282	28
	Volume displacement ltr	10.010	10 011	10.010	10.01
B	Start reading m3	12.64304	12.65331	12.66314	10.01
120 ltr/h	End reading m3	12.65331	12.66314	12.67314	
120 11111	Difference ltr	10.27	9.83	10.00	10.0
	Difference %	2.60%	-1.81%	-0.10%	0.234
	Actual flow rate Itr hour	128.70	128.25	127.79	128.2
ideal <+- 0.5 %	Variance to average	-2.37%	2.04%	0.33% P	140.4
ideal 474 0.3 Fg	variance to average	-2.3 / 76	2.0470	0.5576 [2	233
-	Flow pressure kPa	320	320	320	32
0.5 Qp	Water temperature oC	20.0	20.0	20.0	20
	Test duration sec	483	483	483	48
	Volume displacement ltr	100.220	100.140	100.240	100.20
"A" to "D"	Start reading m3	12.31232	12.41239	12.51239	
750 ltr/hour	End rending m3	12.41239	12.51239	12.61249	
	Difference ltr	100.07	100.00	100 10	100.0
	Difference %	-0.15%	-0.14%	-0.14%	-0.149
	Actual flow rate Itr hour	746.98	746.39	747.13	746.8
ideal <+- 0 2 %	Variance to average	0.01%	-0.00%	-0.00% P	
The same of the sa	- ar mare to average				
	Flow pressure kPa	290	290	290	25
1.00 Qp	Water temperature oC	20.0	20.0	20.0	20
	Test duration sec	246	242	242	24
	Volume displacement ltr	100 090	100.120	100 050	100.08
"A" to "D"	Start reading m3	12.01229	12 11228	12 21236	
1500 ltr/hour	End reading m3	12.11228	12.21236	12.31232	
	Difference ltr	99.99	100.08	99 96	100.0
	Difference %	-0.10%	-0.04%	-0.09%	-0.080
	Actual flow rate ltr hour	1464.73	1489.39	1488.35	1480.7
ideal 0.2 %	Variance to average	0.02%	-0.04%	0.01% P	255
	Flow pressure kPa	860	860	860	86
1.00 Qs	Water temperature oC	19.5	19.5	19.5	19.
	Test duration sec	121	119	120	12
	Volume displacement ltr	100.430	100.420	100.450	100.43
"A" to "D"	Start reading m3	11.70998	11.81054	11.91140	
3000 ltr/hour	End reading m3	11.81054	11.91140	12:01229	
	Difference ltr	100.56	100.86	100.89	100.7
	Difference %	0.13%	0.44%	0.44%	0.34
	Actual flow rate hr hour	2988.00	3037.92	3013.50	3013.0
	Actual flow rate Itr hour	4700.00	18-18-22 F 1 P M	-0.10% P	

REMARKS

Water Meter - Tes Applicable Regulation		Test type:	WRC Project	Print date:	24 March 2000
SABS 1529-1 1994, sect		Customer:	WRC	Print time:	02:23:23 PM
Meter Size:	"3", Qp = 1,5 m3/h "B"	Manufacturer:		Revised	16/06/99
Meter Class:		Motor Tones		File No.:	WRCfit.rex
Magnetic drive	No 3	Meter Type: Flow orientation:		Report No.: Test No:	5421/930507/R29 991901
Route No: Receipt reading:	,	P Group:		1 656 .401	991901
Model:		Working Pressure:			
	Model AI 1		T	*	
Meter Serial #	Model Al I	Test # 1	Test # 2	Test # 3	aver. 1 -3
Test bench position	E3	#3	# 3	#3	111
ELOW DATE	Flow pressure kPa Water temperature oC	320	320 19.5	325 21.5	
FLOW RATE		360	363	362	
(Meter curve)	Volume displacement ltr	10.025	10.019	10.019	
100 ltr/hour	Start reading m3	12.67314	12 68315	12.69317	
100 RC mont	End reading m3	12.68315	12 69317	12.70319	
-	Difference ltr	10.01	10.02	10.02	
	Difference %	-0.15%	0.01%	0.01%	
	Actual flow rate Itr/hour	100.25	99.36	99.64	
	Variance to average	0.11%	-0.05%	-0.05%	
THE RESIDENCE OF THE PARTY OF T		-			
	Flow pressure kPa	320	320	320	320
FLOW RATE	Water temperature oC	19.0	19.0	19.0	19.0
(Meter curve)	Test duration sec	73	73	73	73
	Volume displacement Itr	10.066	10.070	10.070	10.069
500 ltr/hour	Start reading m3	12.61249	12.62271	12.63293	
	End reading m3	12.62271	12.63293	12.64304	
	Difference ltr	10.22	10.22	10.11	10.18
	Difference %	1.53%	1.49%	0.40%	1.14%
	Actual flow rate ltr/hour Variance to average	496.41 -0.39%	496.60	496.60 0.74%	496.54
	Flow pressure kPa Water temperature oC Test duration see Volume displacement ltr Start reading m3 Difference ltr Difference % Actual flow rate ltr/hour Variance to average Flow pressure kPa Water temperature oC Test duration see Volume displacement ltr Start reading m3 End reading m3 Difference ltr Difference ltr Difference ltr Difference ltr Difference %				
	Actual flow rate Itr/hour Variance to average Flow pressure kPa Water temperature oC Test duration sec Volume displacement Itr Start reading m3 End reading m3				
	Difference ltr Difference % Actual flow rate ltr:hour				
	Variance to average				
CONTRACTOR OF THE LABOUR DESIGNATION OF THE PARTY OF THE	THE RESIDENCE OF THE PARTY OF T	NAME AND ADDRESS OF THE OWNER, TH	NAME OF TAXABLE PARTY.	The second second second second second	The second secon

Applicable Regulation SABS 1529-1 1994, section 6.4 and A 4.2h Meter Size:

3

Meter Class: Magnetic drive Route No:

"3", Qp = 1,5 m3/h "B" No

Customer: Manufacturer: Meter Type: Flow orientation: P Group:

Test type:

WRC Project WRC

Print date: Print time:

24 March 2000 02:30:01 PM 15/06/99

Revised WRC-sig-rex File No.: Report No.: 3571/123456/R000/a Test No:

981502

laute No:	3	Flow orientation:		Test No:	981502
eccipt reading:	0.83699	P Group:			
fodel:		Working Pressure:			
Meter Serial #	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1 -3
Test bench position		#3	13	#3	
	Flow pressure kPa	325	325	325	339
	Water temperature oC	20.5	20.0	20.0	22.0
	Test duration sec	3256	3280	3301	3473
	Volume displacement ltr	10.011	10.011	10.011	10.011
10 Uh	Start reading m3	2.59117	2 60104	2.61093	
	End reading m3	2.60104	2.61093	2.62081	
	Difference ltr	9.87	9.89	9.88	9.88
	Difference %	-1.41%	-1.21%	-1.31%	-1.31%
	Actual flow rate ltr/hour		10.99	10.92	10.38
ideal <+= 0.5 %	Variance to average	0.10*%	-0.10%	0.00% P	155
		1	107		
	Flow pressure kPa	325	325	325	325
	Water temperature oC	20.0	20.0	21.0	20.3
	Test duration sec	2303	2311	2305	2306
	Volume displacement ltr	10.013	10.013	10.013	10.013
15 Vh	Start reading m3	2.62081	2.63102	2.64126	
	End reading m3	2.63102	2.64126	2 65155	
	Difference ltr	10.21	10.24	10.29	10.25
	Difference %	1.97%	2.27%	2.77%	2.33%
	Actual flow rate Itrhour		15.60	15.64	15.63
ideal <+- 0.5 %	Variance to average	0.37%	0.07%	-0.43% P	155
	Flow pressure kPa	1 4171	325	325	325
	Flow pressure kPa Water temperature oC	325 20.5	20.5	20.5	20.5
	Test duration sec	1759	1802	1810	1804
20.10	Volume displacement ltr	10.018	2.66185	10.015	10.015
20 l/h	Start reading m3	2.65155		2.67213	
	End reading m3	2.66185	2.67213	2.68245	10.00
	Difference ltr	10.30	10.28	10.32	10.30
	Difference %	2.81%	2.67%	3.05%	2.84%
14. 1 0.44	Actual flow rate ltr hour		20.00	19.92	19.99
ideal <+- 0.5 %	Variance to average	0.03%	0.18%	-0.20% P	155
	Flow pressure kPa	325	325	325	325
	Water temperature oC	20.5	20.5	20.5	20.5
	Test duration sec	1676	1625	1626	1642
	Volume displacement ltr	10.015	10.018	10.018	10.017
22.5 Vh	Start reading m3	2.68245	2.69271	2,70299	10.01
44.5 64		2.69271	2.70299	2.71323	
		10.26	10.28	10.24	10 26
		2.45%	2.62%	2.22%	2.43%
14-1 614	Actual flow rate Ite/hour		22.19	22.18	21.96
ideal <+= 0.5 %	Variance to average	-0.02%	-0.19%	0.21% P	255
	Flow pressure kPa	1251	325	325	325
	Water temperature of	20.0	21.0	21.0	20.7
	Test duration sec	1194	6811	1189	1190
	Volume displacement ltr		10.020	10.020	10.020
30 th	Start reading m3	2.71323	2.72351	2,73360	10.020
20 14		2.72351	2.73360	2.74374	
			10.09		10.17
	Difference Itr	10.28		10.14	1.50%
	Difference %	2.59%	0.70% 30.41	1.20%	30.32
Ideal de O.S.	Actual flow rate Itrhose		0.80%	30.34	
ideal < r = 0.5 %	Variance to average	-1.10%	0.80%	0.30% P	25%

Differential flow ltr h	500	750	1500	3000
Differential pressure kPa				
Manifold pressure kPa				
Pressure test kPa				
Pressure test minutes		See final test sheet		

Applicable Regulation SABS 1529-1 1994, section 6.4 and A 4.2h Meter Size: "3", Qp = 1,5 m3/h Meter Class: "B"

Magnetic drive Route No:

No 3

Test type: Customer: Manufacturer:

Meter Type:

WRC Project WRC

Print date: Print time: Revised File No.: Report No.: Test No: 24 March 2000 02:30:01 PM 15:06:99 WRC-sig-rex 3571/123456/R0000/a

981502

Flow orientation:

eipt reading: del:		Group: orking Pressure:			
Meter Serial #	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1 -3
Test bench position		#3	13	13	
Total Control Property	Flow pressure kPa	325	325	325	
	Water temperature oC	21.0	21.0	21.0	
	Test duration sec	844	856	872	
	Volume displacement ltr	10.021	10.020	10.016	10
40 t/h	Start reading m3	2.74374	2.75381	2.76390	
	End reading m3	2.75381	2.76390	2.77401	
	Difference Its	10.07	10.09	10.11	10
	Difference %	0.49%	0.70%	0.94%	0.7
	Actual flow rate ltr'hour	42.74	42.14	41.35	43
ideal <== 0.5 %	Variance to average	0.22%	0.01%	-0.23% P	155
-	Flow pressure kPa	325	325	325	
	Water temperature oC	20.5	20.0	20.0	
	Test duration sec	728	714	720	-
	Volume displacement Itr	10.019	10.016	10.011	10
50 l/h	Start reading m3	2,77401	2,78404	2.79404	- 10
	End reading m3	2.78404	2.79404	2.80404	
	Difference ltr	10.03	10.00	10.00	10
	Difference %	0.11%	-0.16%	-0.11%	-0.0
	Actual flow rate Itnhour	49.54	50.50	50.05	56
ideal <+= 0.5 %	Variance to average	-0.16%	0.11%	0.06% Pa	
	10-	1477	1321	107	
	Flow pressure kPa	325	325 20.0	325	
	Water temperature oC	479	489	20.0	
	Test duration sec Volume displacement ltr	10.020	10.021	475	10
75 l/h	Start reading m3	2.80404	2.81402	10.021 2.82400	10.
73 88	End reading m3	2.81402	2.82400	2.83398	
	Difference Itr	9.58	9.98	9.98	
	Difference %	-0.40%	-0.41%	-0.41%	-0.4
	Actual flow rate Itrhour	75.31	73.77	75.95	75
ideal < = 0.5 %	Variance to average	-0.01%	0.00%	0.00%	
	Flow pressure kPa	325	325	325	
	Water temperature oC	20.5	20.5	21.0	2
	Test duration sec	358	358	358	
	Volume displacement Itr	10.009	10.009	10.021	10.0
100 l/h	Start reading m3	2.83398	2.84391	2.85386	
	End reading m3	2.84391	2.85386	2.86385	
	Difference ltr	9.93	9.95	9.90	9
	Difference %	-0.79%	-0.59%	-0.31%	-0.56
ideal co. 0 f 9:	Actual flow rate Itr/hour	0.23%	100.65	100.77	100
ideal <== 0.5 %	Variance to average	0.25%	0.03%	-0.25%	
	Flow pressure kPa	325	325	325	
	Water temperature oC	20.5	20.5	20.5	2
	Test duration sec	289	301	300	
	Volume displacement 1tr	10.010	10.011	10 012	10.0
120 l/h	Start reading m3	2.86385	2.87391	2.88387	
	End reading m3	2.87351	2.88387	2.89384	
	Difference Itr	10.06	9.96	9.97	10
	Difference %	0.50%	-0.51%	-0.42%	-0.1-
	Actual flow rate ltr/hour	124.69	119.73	120.14	121
ideal <>- 0.2 %	Variance to average	-0.64%	0.37%	0.28%	pass / fail

Test Date	17/04/98		
Testing Officer	Date://	Manager	Date://
	Signed		Signed

Applicable Regulation

SABS 1529-1 1994, section 6.4 and A 4.2h "3", Qp = 1,5 m3/h "B" Meter Size:

Meter Class: Magnetic drive Test type: Customer: Manufacturer:

Meter Type:

WRC

Print date: 24 March 2000 Print time: 02:30:01 PM

Revised 15/06/99 File No.: WRC-sig-res Report No.: 3571/123456/R000/a

No

Magnetic drive Route No: Receipt reading: Model:	No 3 0.83699	Meter Type: Flow orientation: P Group: Working Pressure:		Report No.: 35 Test No:	571/123456/R000/a
Meter Serial #	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1-3
Test bench position		# 3	# 3	# 3	
	Flow pressure kPa	325	325	325	325
	Water temperature oC	21.0	21.0	21.0	21.0
	Test duration sec	185	180	181	182
	Volume displacement Itr		10.010	10.006	10
200 1/4	Start reading m3	2.89384	2.90384	2.91383	
	End reading m3	2.90384	2.91383	2.92382	
	Difference ltr	10.00	9.99	9.99	9.99
	Difference %	-0.10%	-0.20%	-0.16%	-0.15%
	Actual flow rate linhour		200.20	199.01	197.97
ideal <== 0.2 %	Variance to average	-0.05%	0.05%	0.01% Pr	lss.
ALCOHOL: THE RESERVE OF THE RESERVE	Flow pressure kPa	325	325]	325]	325
	Water temperature oC	21.5	21.5	21.5	21.5
	Test duration sec	71	72	72	72
	Volume displacement ltr	10.061	10.070	10.062	10.064
500 l/h	Start reading m3	2.92382	2.93400	2.94419	10.004
200 04	End reading m3	2.93400	2.94419	2.95448	_
	Difference Itr	10.18	10.19	10.29	10.22
	Difference %	1.18%	1.19%	2.27%	1.55%
	Actual flow rate Ite/hour		503.50	503.10	505.56
ideal <+- 0.2 %	Variance to average	0.36%	0.36%	-0.72% Pr	
	Flow pressure kPa	320	320	320	320
	Water temperature oC	21.5	21.5	21.5	21.5
	Test duration sec	518	532	533	534
/## 1A	Volume displacement Itr		100.140	100.150	100.123
675 Vh	Start reading m3	2,95448	3.05435	3.15436	
	End reading m3	3.05435	3.15436	3.25436	00.04
	Difference ltr	99.87	100.01	100,00	99.96
	Difference %	-0.21%	-0.13%	-0.15%	-0.16%
ideal <== 0.2 %	Actual flow rate lts/hour Variance to average	669.68 0.05%	677.64	676.44 -0.01% Pr	674.57
Ideal 574 U.2 76	variance to average	0.02:0	-0.0376	-0.0170 [1]	155
	Flow pressure kPa	320	330	330	330
	Water temperature oC	23.0	23.0	23.0	23.0
	Test duration sec	468	465	468	467
	Volume displacement Itr	100.240	100.150	100,100	100.163
750 l/h	Start reading m3	3.36375	3.46362	3.56316	
	End reading m3	3.46362	3.56316	3.66279	
	Difference ltr	99.87	99.54	99.63	99.68
	Difference %	-0.37%	-0.61%	-0.47%	-0.48%
	Actual flow rate Itchour		775.35	770.00	772.14
ideal < 0.2 %	Variance to average	-0.11%	0.13%	-0.01% Pa	255
	Flow pressure kPa	315	315	315	315
	Water temperature oC	22.0	22.0	22.0	22.0
	Test duration sec	358	352	357	356
	Volume displacement ltr		100.100	100,100	100.083
1000 Mh	Start reading m3	3.66830	3.76779	3.86733	1110.343
2000 811	End reading m3	3.76779	3.86733	3.96678	
	Difference ltr	99.49	99.54	99.45	99.49
	Difference %		-0.56%	-0.65%	-0.59%
			1023.75		1013.03
	Actual flow rate htr hour	1006.09	1043.731	1009.41	\$10.5000

Differential flow ltrh	500	750	1500	3000
Differential pressure kPa				
Manifold pressure kPa	0	0	0	0
Pressure test kPa				
Pressure test minutes		See final test sheet		

Water Meter - Test Report Applicable Regulation

SABS 1529-1 1994, section 6.4 and A 4.2h

No

0.83699

Meter Size: Meter Class:

Route No:

Magnetic drive

"3", Qp = 1,5 m3/h
"B"

Test type: Customer: Manufacturer: Meter Type:

WRC

Print date: Print time: Revised File No.:

Report No.:

Test No:

24 March 2000 02:30:01 PM 15/06/99 WRC-sig.rex 3571/123456/R000/a

981502

Flow orientation: P Group:

receipt reasong.	0.000077	r consupe
Model:		Working Pressure:

odel:	We	orking Pressure:			
Meter Serial N	Model AI 1	Test # 1	Test # 2	Test # 3	aver. 1 -3
Test bench position		# 3	# 3	#3	
	Flow pressure kPa	300	300	300	300
	Water temperature oC	23.0	23.0	230.0	92.0
	Test duration sec	235	237	236	234
	Volume displacement ltr	100.110	100.150	100.090	100.117
1500 l/h	Start reading m3	3.96678	4.06675	4.16691	
	End reading m3	4.06675	4.16691	4.26709	
	Difference ltr	99.97	100.16	100.18	100.10
	Difference %	-0.14%	0.01%	0.09%	-0.01%
	Actual flow rate Itrhour	1533.60	1521.27	1526.80	1527.20
ideal <+- 0.2 %	Variance to average	0.13%	-0.02%	-0.10% P	
				and the same of th	
	Flow pressure kPa	250	290	290	290
	Water temperature oC	23.0	23.0	23.0	23.0
	Test duration sec	207	203	206	205
	Volume displacement ltr	100.030	100 100	100.060	100.063

	A TOTAL PROPERTY AND ADDRESS.	ALC: U.S.	and the second s	8.77	
	Water temperature oC	23.0	23.0	23.0	23
	Test duration sec	207	203	206	20:
	Volume displacement ltr	100.030	100.100	100.060	100 06
1700 l/h	Start reading m3	4.26709	4.36732	4.46740	
	End reading m3	4.36732	4.46740	4.56769	
	Difference ltr	100.23	100.08	100.29	100.2
	Difference %	0.20%	-0.02%	0.23%	0.14%
	Actual flow rate Ite/hour	1739.65	1775.17	1748.62	1754.36
deal <== 0.2 %	Variance to average	-0.06*6	0.16%	-0.09% Pas	8

ideal <== 0.2 %	Variance to average	0.04%	-0.12%	0.05%	Pass
	Actual flow rate Itrhour	2037.97	2070.41	2071.45	2059 82
	Difference %	0.32%	0.48%	0.28%	
	Difference ltr	100.52	100.55	100.40	100.49
	End reading m3	4.66821	4.76876	4.86916	
2000 Vh	Start reading m3	4.56769	4.66821	4.76876	
	Volume displacement htr	100.200	100.070	100.120	100.130
	Test duration sec	177	174	174	175
	Water temperature oC	23.0	23.0	22.5	22.8
	Flow pressure kPa	270	270	270	270

ideal <== 0.2 %	Variance to average	-0.03%	0.03%	-0.01%	pass / fail
	Actual flow rate Itehour	2613.91	2541.30	2558.04	2570.7
	Difference %	0.61%	0.55%	0.59%	0.58%
	Difference ltr	100.81	100.79	100.78	100.79
	End reading m3	4.96997	5.07076	5.17154	
2500 l/h	Start reading m3	4.86916	4 96997	5.07076	
	Volume displacement Itr	100.200	100.240	100.190	100.210
	Test duration sec	138	142	141	140
	Water temperature oC	23 0	23.0	23.5	23.2
	Flow pressure kPa	840	840	880	85)

	Flow pressure kPa	880	880	880	880
	Water temperature oC	23.5	23.5	23.5	23.5
	Test duration sec	130	131	132	131
	Volume displacement ltr	100.330	100.300	100.240	100.290
2750 Uh	Start reading m3	5.17154	5.27256	5.37354	
	End reading m3	5.27256	5.37354	5.47445	
	Difference ltr	101.02	100.98	100.91	100.97
	Difference %	0.69%	0.68%	0.67%	0.68%
	Actual flow rate Itrbour	2778.37	2756.34	2733.82	2756.06
ideal <++ 0.2 %	Variance to average	-0.01%	0.00%	0.01%	pass / fail

cst.	Place	SABS	retor

Test Date

22/08/97

Testing Officer

Date:

Manager

Date: __/__/__

Signed

Signed ___

SABS Water meter laboratory (012) 428-7089

WRC-sig rex

E20

Applicable Regulation SABS 1529-1 1994, section 6.4 and A 4.2h

Meter Size:

"3", Qp = 1,5 m3/h "B"

Test type: Customer:

W.R.C.

Print date: Print time:

24 March 2000 02:30:01 PM

Meter Class:

Manufacturer:

Revised File No.:

15/06/99 WRC-sig.rex

Magnetic drive Route No:

No

Meter Type: Flow orientation: Report No.: 3571/123456/R000/a Test No: 981502

Receipt reading: Model: P Group: Working Pressure: 0.83699

Meter Serial #	Model AI 1	Test # 1	Test # 2	Test#3	aver. 1 -3
Test bench position		# 3	+ 3	#3	
	Flow pressure kPa	880	880	880	880
	Water temperature oC	23.0	23.5	23.5	23.3
	Test duration sec	117	117	118	117
	Volume displacement ltr	100.440	100.390	100.390	100.407
3000 l/h	Start reading m3	5.62762	5.72890	5.83013	
	End reading m3	5.72890	5.83013	5.93139	
	Difference ltr	101.28	101.23	101.26	101.26
	Difference %	0.84%	0.84%	0.87%	0.85%
	Actual flow rate ltr hour	3090.46	3088.92	3062.75	3080.66
ideal <== 0.2 %	Variance to average	0.01%	0.01%	-0.02%	Pass

	Flow pressure kPa	860	850	840	850
	Water temperature oC	23.5	23.0	23.0	23.2
	Tost duration sec	109	109	110	109
	Volume displacement ltr	100.410	100.400	100.430	100.413
3250 l/h	Start reading m3	5.93139	6.03274	6.13409	
	End reading m3	6.03274	6.13409	6.23547	
	Difference ltr	101.35	101.35	101.38	101.36
	Difference %	0.94%	0.95%	0.95%	0.94%
	Actual flow rate Its hour	3316.29	3315.96	3286.80	3306.29
ideal <++ 0.2 %	Variance to average	0.01%	-0.00%	-0.00%	Pass

Flow pressure kPa	
Water temperature oC	
Test duration sec	
Volume displacement. Itr	
Start reading m3	
End reading m3	
Difference ltr	
Difference %	
Actual flow rate Itr/hour	
Variance to average	

Flow pressure kPa	
Water temperature oC	
Test duration sec	
Volume displacement ltr	
Start reading m3	
End reading m3	
Difference ltr	
 Difference %	
Actual flow rate Itribour	
Variance to average	

	LD. T	 	 _
	pressure kPa	 	
	or temperature oC		
	duration see	 	
Vol	ane displacement ltr		
Start	reading m3		
End	reading m3		
Diff	erence ltr		
Diff	erence %		
Acti	al flow rate ltr/hour		
Var	ance to average		

Differential flow ltr.h	500	750	1500	3000
Differential pressure kPa				
Manifold pressure kPa				
Pressure test kPa				
Pressure test minutes		See final test sheet		

