Geochemical scaling potential simulations of natural organic matter complexation with metal ions in cooling water at Eskom power generation plants in South Africa

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ABSTRACT

The modified database in the pH, redox equilibrium calculations code (PHREEQC) with a Tipping and Hurley database (T_H.DAT) coupled with the Windermere's humic acid model (WHAM) was used to simulate scale formation potential in cooling water circuitry, at Eskom power generating stations in South Africa. This study reports a semi-empirical simulative approach in which organic matter fractions, metals and anions in raw and cooling water were used as modelling experimental inputs. By using the saturation index profiles of Ca^{2+}/Mg^{2+} with fulvic acid in a modified Tipping and Hurley (T_H.DAT) database, fulvate complex species such as CaFulvate, MgFulvate, and geochemical modelling predictions, mineral phases that potentially precipitate are discussed. Speciation calculations showed that the increase in fulvic acid levels decreased saturation indices of scaling metal phases due to reduced levels of Ca^{2+} and Mg^{2+} in the water. Furthermore, if the concentrations of fulvic acid are known, semi-empirical calculations using the geochemical PHREEQC code with a modified T_H.DAT are possible. Consequently, mineral phase equilibria outputs may give an indication of how the pH and temperature is to be manipulated to optimally predict and control the incidence of scaling.

Keywords: mineral phases, PHREEQC, saturation indices, Tipping and Hurley database

INTRODUCTION

Eskom, a power-generating company in South Africa, draws water for cooling turbines mainly from surface water systems. This type of water has high levels of dissolved solids, mainly organic and inorganic compounds (Pather, 2004). The interaction of the various chemical components may produce ions, compounds in solid or liquid phases and complexes. Comprehensive studies have shown that when such water goes through industrial pipes, solid mineral phases, known as scale, form (Zhang et al., 2013, Rosenberg et al., 2012), which compromises water flow efficiency. One challenge, therefore, is the fact that there are dynamic chemical interactions of the water components that lead to changing phases because of changing physico-chemical parameters (such as conductivity, alkalinity and pH) (Brunner, 2014). Current research has shown that natural organic matter (NOM) influences chemical interactions of certain species in natural water. Studies on NOM range from its characterization and fractionation to complexing capacity and degradation. Research has revealed that NOM is a complex matrix with transphilic, hydrophobic and hydrophilic components (Filloux et al., 2012; Zhou et al., 2014).

Evidence indicates that cooling water constituents change as it is recycled over and over, which in turn affects the stability of the NOM-metal complexes and consequently results in changed solubility of the salts present (Hoch et al., 2000, Tipping, 2002). What is not clear is how the fractions of NOM in water and their complexation reaction capacities

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for Ca²⁺ and Mg²⁺ influence pipe scaling. This study sought to provide some answers to this and related questions through geochemical modelling and speciation simulations. One shortcoming, however, is that most geochemical codes do not have comprehensive databases that describe complexation reactions, particularly those that describe NOM fractions. The current study describes (i) the modification of the Tipping and Hurley database with the Windermere Humic Acid Model (WHAM) database (T_H.DAT) to incorporate humate and fulvate equilibrium definitions with Ca and Mg ions, and (ii) speciation calculations generating saturation indices of scaling mineral phases.

Successful modification of the T_H.DAT was achieved by coding log k values for Mg and Ca equilibrium reactions with predominant NOM fractions (fulvates and humates) into it. Stability definitions for these reactions were obtained from risbergfa13.vdb, shmgeneric10.vdb, genericha08.nic and genericfa08.nic databases in Visual MINTEQ version 3.1.1. All these databases are based on the NICA-Donnan model (NIC) (Milne et al., 2003, Koopal et al., 2005, Christensen et al., 1998) and the Stockholm humic model (SHM) (Gustafsson, 2001; Gustafsson and Berggren, 2005; Pourret et al., 2007). To obtain the desired outputs, the modified T_H.DAT was set as the default database in the PHREEQC program and thereafter used for speciation simulations. The simulation mixture comprised of scaling cations (Ca²⁺ and Mg²⁺) and anions (SO₄²⁻, Cl⁻, NO₃⁻) defined as SOLUTION SPECIES. The carbonate concentration was considered as alkalinity measured as HCO, which was also defined in the SOLUTION_SPECIES block. Fulvate-2 and Humate-2, previously defined as SOLUTION_MASTER_ SPECIES in the Tipping and Hurley's WHAM model (2003), generated MgFulvate, CaHumate and MgHumate in addition to other mineral phases. Saturation indices (SI) were calculated using adjusted PHREEQC database (F_H.DAT) to show mineral dissolution or precipitation.

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MATERIALS AND METHODS

The concentrations of the metal ions were determined by inductively coupled plasma optical emission spectrometry (ICP-OES) (Spetro Arcos, with a Cetac ASX-520 autosampler) and the anions in the samples by ion chromatography, IC (ICS – 1500 model) using the Dionex IonPac AS914 (Analytical 4 × 250 mm) column, and the Dionex IonPac AG14 (Guard 4 × 50 mm) column. The LC-OCD analyses were carried out on DOC-Labor LCOCD instrument (Mode 8, Version of 2012-08-27). Fluorescence EEM measurements were conducted using the Aqualog fluorescence instrument (Horiba, New Jersey, USA). The speciation and saturation index simulation results were generated by modelling software, PHREEQC, with an interactive interphase, and a modified Tipping and Hurley (T_H) database.

Sampling and sample preparation

Water samples were collected in 1 000 mL sampling bottles from 4 sampling sites (A: raw, B: clarifier, C: inlet and D: outlet cooling water) (Fig. 1) in the cooling water processes at Kriel and Lethabo power stations. The samples were transported to the laboratory and immediately refrigerated at 4°C.

Instrumentation

pH and conductivity analysis

The pH and conductivity measurements of all samples were done using pH/conductivity meter Model 3540 (Jenway Inc, Essex, CM6 3LB, England) and calibrations performed with calibrating standard solutions (pH = 4.01 and 7.00 at 25°C). The accuracy of the pH measurements was \pm 0.05 pH units. Triplicate readings of each analysis were taken and then the average value used for the analysis.

ICP-OES and ion chromatography analyses

All the samples were filtered through 0.45 μ m syringe filters before analysis. The anions in the samples were analysed by ion chromatography (IC). A mixture of 3.5 mM sodium carbonate (Na₂CO₃) and 1.0 mM sodium bicarbonate (NaHCO₃) was used as the eluent.

LC-OCD analysis

Dissolved organic carbon (DOC) was determined chromatographically using the DOC-labor LC-OCD technique and correlated with the absorbance at 254 nm for specific ultraviolet absorbance (SUVA). Using this technique, a mobile phase was delivered with an HPLC pump (S-100, Knauer, Berlin, Germany) at a flow rate of 1.1 mL·min⁻¹ to an autosampler (MLE, Dresden, Germany, 1 mL injection volume) and the chromatographic column (a weak polymethacrylate cation exchange column, 250mm_ 20 mm, TSK HW 50S, 3000 theoretical plates, Toso, Japan). Before chromatographic separations, water samples were passed through an in-built 0.45 µm membrane filter to remove particulate organic matter. Systematically, the organic carbon detector comes after the non-destructive, fixed wavelength UV-detection (UVD 254 nm, type S-200, Knauer, Berlin, Germany). This LC-OCD procedure was described by Huber



Figure 1

The cooling water process at a typical power generating station at Eskom, South Africa. The symbols, A-D indicate the sampling sites: A - raw water; B - cooling water inlet; C - cooling water at outlet; D - clarifier

et al. (2011). The procedure includes acidification of the water samples at the inlet of the OCD (at a flow rate of 0.2 mL·min⁻¹) to convert carbonates to carbonic acid. This initial stripping process removes all inorganic carbon. Subsequent steps involving analysis of organic carbon were done by wet oxidation. The oxygen required to oxidize DOC comes from water by a process called radiolysis of water at 185 nm. This way, most compounds including fluoro-organic compounds, were oxidized. The organic carbon detector (OCD) calibration was based on potassium hydrogen phthalate. In this case, the carbon mass was used to calibrate the OCD and its extinction coefficient, $\varepsilon = 1.683 \times 10^{-3}$ L·mol⁻¹·cm⁻¹, used to calibrate the UVD (Huber et al., 2011).

Fluorescence excitation-emission matrices (FEEM)

Fluorescence emission excitation matrices (FEEMs) were collected using a Horiba AquaLog Spectrometer (Jvon, New Jersey, USA). No pre-treatment of the samples was applied. Maintaining a common pH between samples ensures that the fluorescence characteristics of the acidic functional groups in humic molecules remain constant. For this reason, all the samples were adjusted to a pH of 7. Collection of intensity values was at 10 nm increments within excitation-emission ranges of 250-450 nm and 300-600 nm, respectively. Scan rate was set to 600 nm·min⁻¹, slit width was set to 10 nm and photomultiplier tube voltage was set to 775 V. Type 1 water at pH of 7 was used as a blank solution. The fluorescence spectrometer used a xenon lamp excitation source and the emission at longer wavelengths was detected at 0.3 nm steps. Further to this, inner-filter correction and Rayleigh scattering was applied to the data.

In this study, fluorescence was carried out under dilute sample conditions, which follows the equation:

$F \propto I_o * Abs_{oV} * \emptyset F \tag{1}$

where I_o is the exciting light intensity, Abs_{ov} is the number of quanta absorbed in the overlap region (OV) and $\emptyset F$ is the ratio of the quanta emitted to the quanta absorbed. The spectra obtained were corrected for instrumental and sample dependent spectral anomalies such as the inner-filter effects associated with sample absorbance of excitation and emission (Rayleigh scattering). Appropriately, spectral data can be compared to standard data and regions in literature and qualitative and quantitative NOM details will be drawn. Figure 2 shows some literature-based spectral regions using defined excitation and emission wavelength boundaries (Gilmore et al., 2003).

Peaks at shorter excitation wavelengths (280 nm) and longer emission wavelengths (> 380 nm) are associated with humic acid–like compounds. This NOM-related spectral information lacks capabilities of quantifying multiple broad-shaped EEM peaks. Chen et al. (2003) postulated that integration beneath EEMs within selected regions would represent cumulative fluorescence responses of NOM with similar properties. This technique shows that the volume Φ_i beneath a region said to be *i* of an EEM be calculated by Eq. 2:

$$\Phi_{i} = \int_{ex}^{x} \int_{em}^{x} I(\lambda_{ex}\lambda_{em}) d\lambda_{ex} d\lambda_{em}$$
(2)

where $d\lambda_{em}$ is the excitation wavelength interval (taken as 10 nm), $d\lambda_{em}$ is the emission wavelength interval (taken as 0.5 nm), and $I(\lambda_{ex}\lambda_{em})$ is the fluorescence intensity at each excitation-emission wavelength pair. The values of Φ_i can be normalized to a DOC concentration of 1 mg·L⁻¹ for comparison of EEMs from different sources of NOM (Zhou et al., 2005).

Via ParaFac modelling, differences in the spectral slopes have been related to the proportional contribution of UV-B



Figure 2 FEEM spectral regions based on reported definite excitation (Ex) and emission (Em) wavelengths (adapted and redrawn from Gilmore et al., 2003)

absorption coefficients to the CDOM spectra which, as literature suggests, is dependent on the different CDOM sources in natural waters (Guéguen et al., 2011). This model factorizes a spectral matrix into three sub-matrices using the same number of factors in Eq. 3. Therefore, the F-EEM data is broken down into a set of tri-linear terms and a residual array.

$$X_{ijk} = \sum_{f=1}^{F} a_{if} b_{fj} c_{kf} + \varepsilon_{ijk} i = 1, \dots, k = 1, \dots, k = 1, \dots, k; \quad (3)$$

Equation 3 is the ParaFac equation in which X_{ijk} is the fluorescence intensity of emission sample *I* at the *j*th emission wavelength and the *k*th excitation wavelength for ParaFac model with *F* number of components. The terms *a*, *b*, and *c* represent the concentration, emission spectra, and excitation spectra, respectively, of the different fluorophores. The a_{if} term is directly proportional to the concentration of the *f*th analyte of the *i*th sample, while b_{ji} and c_{kf} are scaled estimates of the emission and excitation spectra at wavelengths *j* and *k*, respectively, for the *f*th analyte. The ε_{ijk} term represents any unexplained signal resulting from residual noise or un-modelled variability (Gentry-Shields et al., 2013). Evidence suggests that with the ParaFac model, four fluorescent components are identifiable: a protein-like component, soluble microbial by-product-like component, non-humic-like component and fulvic-like component (Guo et al., 2012).

Modelling using PHREEQC-Interactive

The geochemical code, PHREEQC, was used to calculate the aqueous speciation and saturation indices of different mineral phases. The phases included aragonite, calcite, gypsum, magnesite, anhydrite and dolomite. During the assessment of the impact of humic substances on speciation and saturation indices, PHREEQCI databases were modified before calculations. PHREEQC Version 3 implements many types of aqueous models, among them the following: ion-association aqueous models (the Lawrence Livermore National Laboratory model and WATEQ4F), a Pitzer specific-ion-interaction aqueous model, and the SIT (Specific ion Interaction Theory) aqueous model (Parkhurst and Appelo, 2013). Using these aqueous models, PHREEQC is able to carry out the following simulations: ion speciation (output including saturation indices), batch-reaction modelling (including equilibrium phases), surface complexation and ion exchange, reaction (addition/removal of specified elements), mixing waters and changing temperature, transport modelling, advection with reactions with and without dispersion, and inverse modelling, and can calculate reactions that account for changes in composition of water along a flow path (Parkhurst and Appelo, 2013).

Database modification

The specific database used in PHREEQC for the simulations is based on various approaches such as (i) the ion association approach (these include *phreeqc.dat, wateq4f.dat, minteq.dat, llnl.dat, iso.dat* and *phreeqd.dat* (Charlton and Parkhurst, 2011); (ii) the diffusion coefficients: multicomponent diffusion, specific conductance; iii) molar volumes for calculation of density; and iv) the Pitzer specific interaction approach – *Pitzer.dat.* Various databases are based on the equations that define activity coefficients for model solutions and reactions and are discussed in this section. For example, the Lawrence Livermore National Laboratory aqueous model (LLNL) uses the following expression (Eq. 4) for the log (base 10) of an activity (Charlton and Parkhurst, 2011):

$$\log \gamma = \frac{A\gamma^{z^2}\sqrt{I}}{1+a_i^0 B_\gamma \sqrt{I}} + BI$$
(4)

where A_{γ} is the Debye-Hückel *A* parameter corresponding to -**dh_a**, B_{γ} is the Debye-Hückel *B* parameter corresponding to -**dh_b**, *B* is the Debye-Hückel *B*- dot parameter corresponding to -**bdot**, a_i^{0} is the hard-core diameter, which is specific to each aqueous species, and *I* is the ionic strength. The LLNL_ AQUEOUS_MODEL_PARAMETERS data block defines A_{γ} , B_{γ} and *B* as functions of temperature (Charlton and Parkhurst, 2011).

The Pfizer database is based on the Pfizer activity coefficients. Equation 5 shows the expression for a Pitzer parameter, P with T as the temperature in Kelvin, and T_r as the reference temperature (298.15 K). If less than 6 parameters are defined, the undefined parameters are assumed to be zero. When modifying a Pitzer aqueous interaction parameter, care is needed to ensure thermodynamic consistency among all the parameters. If the same type of parameter with the same set of species is redefined, even if the order of the species is different, then the previous definition is removed and replaced with the new definition (Charlton and Parkhurst, 2011).

$$P = A_0 + A_1 \left(\frac{1}{r} - \frac{1}{T_r}\right) + A_2 \ln\left(\frac{T}{T_r}\right) + A_3 \left(T - T_r\right) + A_4 \left(T^2 - T_r^2\right) + A_5 \left(\frac{1}{T^2} - \frac{1}{T_r^2}\right)$$
(5)

Carefully, therefore, the humate and fulvate thermodynamic definitions were incorporated into a Tipping and Hurley database with a WHAM (T_H.DAT) (Tipping, 2002), which defines the LLNL and the Pfizer databases. Table 1 shows the log *k* values for equilibrium phase equations of the reactions incorporated into the T_H.DAT database together with their stability constants, all drawn from visual MINTEQ v 3.1.1. For these reactions, the phases were defined as SOLUTION_SPECIES in T_H.DAT.

The simulation mixture comprised of scale-forming cations (Ca²⁺ and Mg²⁺) and anions (SO₄²⁻, Cl⁻, NO₃⁻) defined as SOLUTION_SPECIES. The carbonate concentration was considered as alkalinity measured asHCO₃⁻ which was also defined in SOLUTION_SPECIES block. Fulvate-2 and Humate-2, have been previously defined as SOLUTION_MASTER_SPECIES in the Tipping and Hurley WHAM model (2003). The modified T_H.DAT incorporates log *k* values from *risbergfa13.vdb*, *shmgeneric10.vdb*, *genericha08.nic* and *genericfa08.nic* databases in visual MINTEQ version 3.1. These values define the equilibrium phase equations of NOM (humic and fulvic acid) with Mg²⁺ and Ca²⁺ that give rise to CaFulvate, MgFulvate, CaHumate and MgHumate (Fig. 3).

TABLE 1 Equilibrium phase equations defined in T_H.DAT as SOLUTION_SPECIES using the NICA-Donnan visual MINTEQ				
Phase	Equilibrium reaction	Log k		
#CaFulvate	Ca^{+2} + Fulvate ⁻² = CaFulvate	-3		
#MgFulvate	$Mg^{+2} + Fulvate^{-2} = MgFulvate$	-2.4		
#CaHumate	Ca^{+2} + Humate ⁻² = CaHumate	0.43		
#MgHumate	Mg^{+2} + Humate ⁻² = MgHumate	0.60		



Figure 3

Modification of the Tipping and Hurley database with WHAM (T_H.DAT) to include humates and fulvates. The speciation outputs of equilibrium reaction definitions in Table 1 are shown under modified T-H.DAT.

Mineral saturation

The pH, alkalinity, metal cations and anions were modelled together with organic components (fulvates) using a fulvateadjusted T_H database. The input-output geochemical execution processes on the PHREEQC code are summarised in Fig. 4. To show mineral dissolution or precipitation, saturation indices (SI) were calculated. Herein, a general reaction (Eq. 6), describes super-saturation which is the key parameter that determines precipitation. The saturation ratio (S) is described as the ratio of the ionic activity product (IAP) to the equilibrium constant (*Ks*) (Eq. 7).

$$A^- + B^+ = AB + g + l \tag{6}$$

where A⁻ is the anion being equilibrated ($A^- = (SO_4^{2-}, Cl^-, NO_3^{-}, CO_3^{2-}, PO_4^{3-})$, B^+ is the metal cation, *AB* is the mineral phase formed and *g* and *l* are any gas or liquid phases, respectively.

$$S = \frac{IAP}{K_s} = \frac{[A^-][B^+]}{K_s}$$
(7)

A value of S < 1, indicates an under-saturated solution, S = 1 shows a solution in equilibrium with the solid, while S > 1 shows



Figure 4

A scheme on geochemical modelling processes. The PHREEQCI processes with a modified T_H database typify these processes

a supersaturated solution, which leads to precipitation/scaling. Saturation indices (SI) are defined as SI = $\log_{10}(S)$, so that an equilibrium situation corresponds to SI = 0, and under-saturation and super-saturation shown by SI < 0 and SI > 0, respectively.

A very high or very low SI does not always indicate 'extreme' conditions but may merely be a mineral that is less reactive. From a geochemistry perspective, reactive minerals are those that dissolve in water or precipitate from water during the residence time in the water (Peters, 2009). A general flow scheme on geochemical modelling is given in Fig. 4.

RESULTS AND DISCUSSION

The FEEM spectral signatures, LC-OCD, IC, ICP-OES results together with speciation simulations are presented for raw, clarified and cooling water from Kriel (K) and Lethabo (L) power

stations. This study focuses on raw and cooling water at the outlet point to explain potential scaling in water pipe circuitry. Using pH values (Table 2), alkalinity, alkaline earth metal cations (Ca²⁺, Mg²⁺) and anions (SO₄²⁻, Cl⁻, NO₃⁻, CO₃²⁻, PO₄³⁻), various temperature and NOM (fulvic acid) dependent simulations were carried out. The relatively similar raw water characteristics obtained in this study confirmed water use from the same source, the Vaal River. Fundamental characteristics of water, which were used as inputs in the PHREEQC simulations, are shown in Table 2.

Characterization and quantification of NOM

Identification of humic substances

The improved humic substances (HS) diagram (HS-diagram), reveals the aromatic character (*x*-axis) of NOM fractions as a

TABLE 2 Main characteristics of raw and cooling water in the cooling water processes (CWPs)								
Characteristic	Lethabo Water			Kriel Water				
	Raw	Clarifier	Inlet	Outlet	Raw	Clarifier	Inlet	Outlet
рН	10.22	9.05	9.60	8.91	9.97	9.74	10.46	9.69
Conductivity (S/m)	0.18	4.63	4.05	4.67	0.28	3.49	3.25	3.46
Common anions (IC)) in mg·L ⁻¹							
Fluoride	0.60	2.11	2.07	2.31	0.65	2.60	1.15	3.06
Bromide	ND	158.95	159.57	166.41	ND	47.42	43.85	41.75
Sulphate	0.09	5.595	4.11	5.98	0.20	3.442	5.08	3.12
Scaling metals (ICP-OES/MS) in mg·L ⁻¹								
Ca	7.85	34.53	38.94	37.81	11.25	142.95	154.6	158.2
Mg	15.46	212.1	231.9	236.0	17.41	97.43	111.9	115.3
Ва	0.05	0.90	0.12	0.12	0.06	0.13	0.22	0.23

function of their molecularity (y-axis) (Fig. 5a). This diagram is a plot of the spectral absorption coefficient (SAC) to the organic carbon (OC) ratio (aromaticity) of a HS-fraction against its nominal molecular weight $(M_{..})$ (Huber et al., 2011). Accordingly, the curved boundaries define the region where the humic substances are characterized. The humic substances area was developed using fulvic and humic acid characteristics of water samples from different sources discussed in Huber et al. (2011). As reported in Huber et al. (2011), the humic acid (HA) and fulvic acid (FA) standard (II) isolates of the International Humic Substances Society (IHSS) were used to calibrate the HS molecular weights, prior to all characterizations. In the current study, raw and cooling water samples from Kriel and Lethabo power stations, were characterized. The results obtained showed that raw, clarifier and cooling water (inlet and outlet) from Kriel (shown by K) and Lethabo (shown by L) consists mainly of pedogenic fulvic acids (Fig. 5a). The fulvic acid character increased in the order of E > A > G, B and C > H and F > D. The raw water data points A and E, from Kriel and Lethabo, respectively, are close to each other in the HS-diagram (Fig. 5a). This confirms the common source of cooling water used at these Eskom power stations, i.e., the Vaal river. The FA reported in this study is in close agreement with data reported by Huber et al. (2011), regarding the characteristics on the HS-diagram FA obtained from the river Rhine, river Seine and Steinbach surface water (Huber et al., 2011). However, the FA obtained from our study differs from the FA reported by Huber et al. (2011) on data obtained for river Westend, Lake Sosa, Lake Galilee and Caspian Sea waters. This variation in results further reveals the difference in surface origin of the FA obtained in our study, which was predominant in the cooling water analysed in this study.

Quantification of NOM fractions

Natural surface waters exhibit 5 distinct peaks corresponding to LC-OCD elutes of different NOM fractions, namely: (i)







Figure 5a

The HS-diagram for humic fractions in cooling water samples from the Kriel (K) and Lethabo (L) power stations. Aromaticity of aquatic humic substances is measured as the SAC/OC ratio, which is plotted against molecularity (Mn values (nominal molecular weights)). (A: K-Raw; B: K-outlet CW; C: K-inlet CW; D: K-clarifier; E: L-Raw; F: L-clarifier; G; L-inlet CW; H: L-outlet CW). The calibration water sources are adapted from by Huber et al., 2011.

biopolymers; (ii) humic substances; (iii) building blocks; (iv) low molecular weight acids and (v) low molecular weight neutrals. The major components of the humic substances' fraction, the HA and FA elute at 43.4 and 46.7 min, respectively (Huber et al., 2011). Fig. 3b shows chromatograms corresponding to the NOM fractions analysed by LC-OCD.

Table 3 summarizes the LC-OCD quantitative results, based on the raw and cooling water samples from the two power stations. These results include the humic substances which were predominantly fulvic acid, shown in Fig. 5b. For all samples, the humic substances fraction quantities did not differ significantly with total dissolved organic carbon (DOC) ($r^2 = 0.01677$, p < 0.05, ANOVA). For example, the percentage HS concentration to the total DOC in the raw water was 88.4% and 89.5% for samples from Kriel and Lethabo power stations, respectively. Separately, a similar observation was made using cooling water, i.e., 87.8% and 83.5% for Kriel and Lethabo, respectively. However, the raw and cooling water HS fractions from the power stations differed significantly ($r^2 = 0.95$, p < 5, ANOVA).

Table 3 also shows the SUVA values corresponding to the various samples. NOM is hydrophilic (HPI) if the specific UV absorbance at λ_{254} (SUVA) value < 2 (an indication of non humic substances), hydrophobic (HPO) with a SUVA value > 4 (an indication of humic substances) and is transphilic (TPI, a mixture of both HPO and HPI) if $2 \le SUVA \le 4$. In the present study, the SUVA values of the water samples generally show that the nature of humic substances is highly aromatic. This is supported by the high percentage of HS in dissolved organic carbon (DOC). Similar studies have shown that surface water from different sources contains a NOM matrix comprising of transphilic, hydrophobic and hydrophilic compounds (Filloux et al., 2012, Zhou et al., 2014). The percentage of humic substances reported by Zhou et al. (2014) (84%) agree with the LC-OCD results obtained in this study for the raw and cooling water processes (ranging from 80-90%).

FEEM characterization of NOM

Typical FEEM spectra of cooling water used at the Kriel power station are presented in Fig. 6. Generally, the observed excitation (EX) and emission (EM) spectra for water samples confirmed intense fulvic acid and humic acid activities. These

Figure 6

Typical fluorescence excitation-emission matrices of raw water (a), clarified water (b) and cooling water (c). The x-axis shows the range of excitation (EX) wavelength (220–350 nm) and the y-axis shows the emission (EM) wavelength range (220–610 nm)



TABLE 3 Structural qualities of DOC and quantity of HS obtained with LC-OCD for Kriel (K) and Lethabo (L) power stations (*% HS is calculated as (HS/DOC) × 100; *BBs represents building blocks)						
Sample	DOC (mg·L⁻¹)	HS (mg·L⁻¹)	%* HS	BBs as % of HS	SUVA SAC/DOC (L·mg ⁻¹ ·m ⁻¹)	
K-Raw	5.934	5.244	88.4	12.548	5.18	
K-CWO	49.290	43.282	87.8	13.534	4.36	
K-CWI	47.023	40.574	86.3	15.769	4.40	
K-Clarifier	81.422	68.849	84.6	14.715	3.40	
L-Raw	4.022	3.599	89.5	10.475	6.58	
L-Clarifier	45.902	36.741	80.0	23.162	3.36	
L-CWI	25.830	21.714	84.1	18.698	4.97	
L-CWO	38.775	32.378	83.5	18.374	3.93	

observations complement the LC-OCD results presented in Table 3. The spectral signatures, as revealed by FEEM (Fig. 6), showed intense activity of HS at λ_{EX} 250–290/ λ_{EM} 350–500 nm, which further confirmed the predominance of fulvic acid in the NOM. The fulvic acid FEEM spectral regions have been reported elsewhere (Ahmed et al., 2014).

The observed raw and cooling water characteristics of NOM using LC-OCD and FEEM (found to be predominantly FA), and the quantitative measurements of HS (established to be FA), formed the basis of modelling discussions under the geochemical sub-heading. These include database modifications and the use of the PHREEQC code to include FA equilibrium reactions with selected cations.

Geochemical modelling

At ambient temperature (25°C), the selected minerals (aragonite, dolomite, gypsum, calcite and magnesite) showed higher dissolution than precipitation (Fig. 7). These results were further simulated in an extended range of temperatures and the concentration of fulvic acid. Mineral phase modeling, using F H.DAT, showed distinct saturation patterns. Saturation indices of selected phases are discussed in this article, including: the two polymorphs of calcium carbonate, namely; aragonite (CaCO₂) and calcite (CaCO₂), anhydrite (CaSO₄), gypsum (CaSO₄·2H₂O), dolomite CaMg(CO₂)₂ and magnesite (MgCO₃). Both alkalinity defined as HCO₃ and sulphurcompounds in the form of SO₄²⁻ values were calculated as averages of raw and cooling water from Lethabo power station. From Fig. 7, the saturation levels revealed variations depending on the source of water. This conforms to what is expected as the cooling water evaporates. As the water gets recycled over and over, its components concentrate. The influence of temperature and concentration of humic substances on formation and saturation of these mineral phases are modelled in this section.

Temperature-dependence mineral simulations

Temperature simulations revealed 2 types of mineral phase occurrences: (i) mineral phases below and above the saturation lines (Fig. 8) showing under-saturation and supersaturation (calcite, aragonite, dolomite and magnesite), respectively; (ii) mineral phases showing under-saturation only (anhydrite and







Figure 8

Predictive saturation indices of mineral assemblages based on temperature, viz, calcite, aragonite, dolomite, anhydrite, gypsum and magnesite (K and L represent water drawn from Kriel and Lethabo, respectively)

gypsum). The saturation indices of minerals were calculated from the F_H.DAT. Calcite (CaCO₂) was found to have higher saturation indices than aragonite (CaCO₃). For example, in almost all (except raw water samples) calcite showed supersaturation at lower temperatures than aragonite. A very specific illustration is the precipitation of calcite and aragonite in the Kriel clarifier (K-clarifier) and Kriel cooling water outlet (K-CWO), from 15°C and 30°C, respectively (Fig. 8 Calcite, and Fig. 8 Aragonite). It is important to mention that crystals of CaCO, exist in different polymorphs, i.e., calcite, aragonite and vaterite. Calcite is the most stable of the three while vaterite is the least stable. Ideally, they form under different conditions, for the same amounts of inputs (Wada et al., 2013). Aragonite is a high-pressure phase which changes to calcite at ambient conditions. Its precipitation is dependent on pH, temperature, super-saturation and CO₂ content.

The relatively high degree of under-saturation of gypsum (CaSO₄·2H₂O) and anhydrite form (CaSO₄) compared to other mineral phases is likely to be due to the low concentration of sulphate ions in the cooling and raw water samples (Fig. 8 gypsum; Fig. 8 anhydrite). Gypsum and anhydrite dissolution were apparent in most of the water samples, thus contributing free Ca²⁺ that enhances calcite precipitation, a phenomenon called common ion driven precipitation (CIDP). We noted that calcium concentrations are controlled by calcite and aragonite dissolution. Furthermore, the dynamics of Ca complexation and dissolution govern its pH-dependent equilibria (Pokrovsky et al., 2009). Pokrovsky et al. (2009) provided a detailed argument on the dissolution kinetics and precipitation of dolomite and magnesite, in addition to calcite, as a function of pH, temperature and pressure. They noted that the rate constants of dissolution of these minerals increase with increase in pH and temperature. This agrees with the temperature-dependent simulation results in this study.

Speciation simulations based on NOM (fulvic acid)

The concentrations of fulvic acid were determined to be in the range 3.5 to 81.5 mg·L⁻¹, viz, (i)) Lethabo had concentrations as follows: raw 4.022 mg·L⁻¹, clarifier 45.902 mg·L⁻¹, CWI 25.830 mg·L⁻¹ and CWO 38.775 mg·L⁻¹, compared to (ii) Kriel's raw 5.934 mg·L⁻¹, clarifier 81.422 mg·L⁻¹, CWI 47.023 mg·L⁻¹ and



Figure 9

Extrapolated mineral phase curves based on raw water concentrations at Kriel. Various exponents of the experimental fulvic acid concentrations were input parameters into the PHREEQC SOLUTION_ SPECIES using the F_H.DAT.

http://dx.doi.org/10.4314/wsa.v44i4.19 Available on website http://www.wrc.org.za ISSN 1816-7950 (Online) = Water SA Vol. 44 No. 4 October 2018 Published under a Creative Commons Attribution Licence CWO 49.290 mg·L⁻¹ (Table 3). Raw water fulvics were compared with those from the clarifier as well as those from the cooling water tower. As expected, the results showed that the fulvics from the cooling tower were found to be less than a tenth of those from the clarifier. This may be attributed to the fact that recycled water volumes keep decreasing due to the evaporative processes in the cooling water chambers and this concentrates the humic substances (Pather, 2004). Various exponents of the experimental fulvic acid concentrations were inputted to the PHREEQC SOLUTION_SPECIES using the F_H.DAT and the results are presented in Figs 9 and 10.

How available and reliable are the thermodynamic and equilibrium definitions of NOM in the existing databases? Undoubtedly, no single modification would suit all organic compounds. Huber et al. (2012) agree with this. In their simulations, they chose to pick thermodynamic definitions of volatile fatty acids (acetate, propionate, butyrate and lactate) from MINTEQ.V4.DAT and included them in the PHREEQC code with interactive interface (PHREEQCI) database (Huber et al., 2012). Therefore, to answer the question, the F_H.DAT was constructed using available thermodynamic definitions for the Ca and Mg-fulvate equilibrium phases in Visual MINTEQ.v3.1.1. This work drew up specific species-oriented modifications on the premise that variability of both the physico-chemical conditions and the wide range of compounds in cooling water play a critical role in data generation.

Based on the expanded fulvic acid simulations from our study, the effect of fulvate ions as defined in the EQUILIBRIUM_PHASE and SOLUTION_MASTER_SPECIES in the F_H.DAT was investigated. Results show that by changing the fulvic acid concentrations in cooling water processes, one can alter scaling indices of mineral phases significantly (Figs 9 and 10). These figures are extracts of the raw and cooling water results at Kriel power station. This reduction may be attributed to the formation of the defined complexes between Ca/Mg and fulvic acid, viz, MgFulvate and CaFulvate.

Scale control modelling studies

In this article, the composition of scale in pipes, with physicochemical conditions determined, is given in Table 4. The experimental results shown in Table 4 were obtained from



Figure 10

Extrapolated mineral phase curves on a reduced scale on x-axis showing the concentration of fulvic acid (0–6 000 mg·L⁻¹)

analysis of a scale sample obtained from cooling water pipes at Lethabo. Accordingly, the results showed varied concentrations of elements in the order of Zn > Al > Ca > Mg for the 4 metal ions under consideration.

The second step was to accurately determine the content of scaling metals and other trace elements in water. The fundamental objective in the current context is to keep Ca/Mg ions in solution (complexed form). Therefore, it was important to include organic compounds in the PHREEQC databases and simulate scale formation under different conditions (shown in the methodology section). In that section, a typical illustration

TABLE 4 Selected sample XRF results of the components of scale obtained from Lethabo cooling water pipes						
Mineral phase	Formula	% by mass	Total			
Zn mineral phases						
Smithsonite	Zn(CO ₃)	0.4	48.5			
Zinc phosphate	Zn(PO ₃) ₂	28.3				
Zinkosite, syn	ZnSO ₄	19.8				
Al mineral phases						
Berlinite; berlinite,	Al(PO ₄)	35.6	36.9			
Diaspore, syn	AlO(OH)	1.3				
Ca mineral phases						
Calcium iron(II) oxide	CaFeO ₂	5.5	14.1			
Gypsum	CaSO ₄ ·2H ₂ O	0.6				
Calcium silicide	CaSi ₂	0.3				
Aragonite	Ca (CO ₃)	7.5				
Dolomite	Ca Mg $(CO_3)_2$	0.2				
Mg mineral phases						
Magnesite, syn	Mg (CO ₃)	0.5	0.7			
Dolomite	Ca Mg $(CO_3)_2$	0.2				

of precipitative and complexation processes has been discussed using the context of fulvic acid interactions with metal cations.

Table 5 shows potential scaling potentials of selected mineral phases of Ca and Mg in water; aragonite (CaCO₃), artinite (MgCO₃:Mg(OH)₂:3H₂O), brucite (Mg(OH)₂), calcite (CaCO₃), dolomite (CaMg(CO₃)₂), dolomite(d) CaMg(CO₃)₂, huntite (CaMg₃(CO₃)₄), hydromagnesite (Mg₅(CO₃)₄(OH)₂:4H₂O) and magnesite (MgCO₃). From this study, the interaction between calcium and carbonate ions is defined to influence scaling in water pipes. The saturation indices of aragonite and calcite (polymorphs of CaCO₃) are positive throughout the recycle water processes (in raw and in cooling water). From the study, these polymorphs remained relatively stable throughout the recycle processes.

The third step is to consider the current state Ca binding to fulvic acid, in raw water compared to recycled cooling water. For instance, the molality values of CaFulvate are lower (viz; 4.6×10^{-13} and 1.5×10^{-11}) in raw water at Lethabo and Kriel, respectively. This complex is 100-fold higher in cooling water than in raw water (Table 6). A similar scenario is experienced with MgFulvate. This phenomenon explains the fact that cooling recycled volumes have reduced precipitation potentials for Mg and Ca. This leads to the conclusion that manipulation of physicochemical parameters enhances complexation of Ca and Mg, which inhibits complexation of non-scaling metals while reducing the components that oxidise, which is critical in scale control.

TABLE 6 Summary of the Ca/Mg fulvate complexes (in mols) in raw and cooling water						
	Lethabo station Kriel station					
Complexed species	Raw water	Cooling water	Raw water	Cooling water		
Fulvate-2	5.5 10-6	5.0×10^{-5}	8.1×10^{-6}	1.1×10^{-4}		
HFulvate-	$5.3 imes 10^{-11}$	$7.4 imes 10^{-10}$	$1.5 imes 10^{-11}$	$2.8 imes 10^{-10}$		
CaFulvate	4.6×10^{-13}	1.4×10^{-11}	1.1×10^{-12}	1.3×10^{-10}		
MgFulvate	6.7×10^{-12}	$6.1 imes 10^{-10}$	1.2×10^{-11}	$6.8 imes 10^{-10}$		

TABLE 5 Saturation indices of various mineral phases of Ca and Mg					
	Lethabo station Kriel station				
	Saturation indices				
Mineral phase	Raw water	Cooling water	Raw water	Cooling water	
Anhydrite (CaSO ₄)	-5.8	-3.6	-5.3	-3.2	
Aragonite (CaCO ₃)	0.9	0.7	1.0	1.8	
Artinite (MgCO ₃ :Mg(OH) ₂ :3H ₂ O)	0.6	-0.6	0.1	0.8	
Brucite (Mg(OH) ₂)	0.2	-1.3	-0.2	-0.1	
Calcite (CaCO ₃)	1.1	0.9	1.1	2.0	
Dolomite $(CaMg(CO_3)_2)$	2.8	2.9	2.8	4.2	
Dolomite(d) CaMg(CO ₃) ₂	2.3	2.4	2.3	3.6	
Epsomite (MgSO ₄ :7H ₂ O)	-7.5	-4.8	-7.0	-5.4	
Gypsum (CaSO ₄ :2H ₂ O)	-5.6	-3.4	-5.0	-3.0	
Huntite ($CaMg_3(CO_3)_4$)	2.0	2.6	1.9	4.3	
Magnesite (MgCO ₃)	1.2	1.5	1.1	1.6	
Nesquehonite (MgCO ₃ :3H ₂ O)	-1.2	-0.9	-1.3	-0.8	
Portlandite (Ca(OH) ₂)	-6.3	-8.3	-6.6	-6.1	

Given the results in Tables 5 and 6, we can conclude that complexation between Ca/Mg cations and fulvates could be linked to saturation indices in explaining the scaling potential. Saturation index results show that only the values in raw water samples are slightly different. However, the fact is that the incorporation of the equilibrium equations for Ca and Mg with fulvates into the PHREEQC databases, could offer a special link that explains simultaneous complexation and precipitation reactions in fresh waters used for industrial purposes. Modelling the formation of these discrete chemical complexes showed a reduction in the concentration of free Ca and Mg ions in solution, hence decreased scaling potential. In addition, the study has shown that the concentrations of fulvic acid and temperatures may be manipulated, and using the geochemical code PHREEQC, the incidence of scaling could be predicted and controlled.

CONCLUSIONS

The HS-diagram revealed the predominance of the fulvic acid fraction of NOM in raw and cooling water. For all samples, the fulvic acid fraction did not differ significantly relative to total dissolved organic carbon. In addition, the spectral EEM signatures, showed intense activity of HS at $\lambda_{_{\rm EX}}$ 250–290/ $\lambda_{_{\rm EM}}$ 350-500 nm, which confirmed the predominance of fulvic acid in NOM. Using the PHREEQC code, the Tipping and Hurley database (T_H.DAT) was successfully modified by including Mg and Ca complexation equilibrium equations with the fulvate ion. This was achieved by incorporating Fulvate-2 complexation equilibria in the SOLUTION_MASTER_SPECIES block and defining it as SOLUTION_SPECIES. Both the humates and fulvates were incorporated in the T_H.DAT database correctly and were able to generate outputs on the PHREEQC code. As a result, new complexation the Ca-fulvate and Mg-fulvate mineral phase outputs were obtained and related to the scaling potential of Ca/ Mg. Overall, the entire study has shown that if the concentrations of organics (such as fulvic acid) are known, the conditions that favour their complexation with Ca/Mg could be manipulated appropriately to control the incidence of scaling in pipe circuitry.

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