Municipal sludge as source of nitrogen and phosphorus in perennial pasture *Eragrostis curvula* production: Agronomic benefits and environmental impacts

Eyob H Tesfamariam¹*, John G Annandale¹, Joachim M Steyn¹, Richard J Stirzaker² and Ikenna Mbakwe¹ ¹Department of Plant Production and Soil Science, University of Pretoria, Private Bag X20, 0002, Pretoria, South Africa ²CSIRO Land and Water, PO Box 1666, ACT 2601, Australia and CRC for Irrigation Futures, PO Box 56, Darling Heights, Queensland, Australia 4350

ABSTRACT

Land application of sludge has been shown to improve soil properties and aid crop growth, but the possibility of constituent nutrients such as nitrogen and phosphorus reaching environmentally toxic levels has caused governing authorities to set limits to how much sludge can be applied to agronomic land. The high nitrogen utilisation potential of pasture grasses suggests that more sludge can be used in this cropping system without the risk of excess nitrates. This study investigates the effect of exceeding the South African sludge application limit on hay yield, soil nitrates and phosphorus. Field plots were arranged in a complete block design comprising 4 replications of 4 treatments planted to Eragrostis curvula. The treatments consisted of 0, 4, 8 and 16 Mg-ha⁻¹ anaerobically digested sludge. Soil samples were collected before treatment application and at the end of each growing season for N, P, NO₄, NH₄, and Bray-1P analyses. Plant samples were collected at flowering stage for hay yield and N and P uptake determination. Statistical analyses were conducted using analysis of variance (ANOVA) and general linear model (GLM) procedures of Windows SAS 9.0 to evaluate the effect of sludge application rates on hay yield. Results over 4 growing seasons indicate that exceeding the recommended limit increased hay yield by 4% in a dry season (11.7 vs. 12.36 Mg·ha⁻¹) and by 16% in a wet season (14.19 vs. 17.31 Mg·ha⁻¹) and also increased nitrogen uptake by 15%. Sludge applied at double the recommended limit did not cause the accumulation of nitrate and ammonium in the soil, however, both total and Bray-IP were doubled. The study shows that the potential long-term environmental risk of doubling the sludge application rate norm would be from labile P accumulation in the soil profile despite a sludge P:Fe molar ratio of less than unity.

Keywords: sludge, Eragrostis curvula, nitrogen, phosphorus, leaching

INTRODUCTION

Use of sewage sludge on agricultural land has been practised for a long time around the world, and has been shown to have several benefits. Sludge acts as a source of essential crop nutrients (Smith and Tibbett, 2004; Ferreiro-Domínguez et al., 2011), stimulates microbial activity (Boyle and Paul, 1989; Lakhdar et al., 2010), immobilises toxic elements in soil (Neunhäuserer et al., 2001), improves soil structure, and minimises soil erosion and runoff (Ojeda et al., 2008).

However, nutrients applied above a crop's nutrient requirement can be detrimental to plant growth and may ultimately pollute water bodies (Neal et al., 2002). Excess nitrates from sludge may be leached down and contaminate groundwater or be washed out into water bodies and exacerbate algal blooms. Excess phosphorus washed away from the soil may also enhance the rate of eutrophication in nearby water bodies (Xie et al., 2011). In addition, waste products from cities and industrial areas contain pathogens, toxic elements and organic contaminants which can pose a serious health hazard especially when they enter the food chain. For these reasons, many countries have developed sewage sludge guidelines to optimise agricultural benefits without compromising the environment.

To whom all correspondence should be addressed.
+27 12 420 4724; fax: +27 12 420 4120;

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http://dx.doi.org/10.4314/wsa.v39i4.9 Available on website http://www.wrc.org.za ISSN 0378-4738 (Print) = Water SA Vol. 39 No. 4 July 2013 ISSN 1816-7950 (On-line) = Water SA Vol. 39 No. 4 July 2013 In South Africa, where beneficial agricultural use of sludge accounts for only 28% of the total sludge produced from South African wastewater treatment plants, the Water Research Commission initially pegged sludge application on land at not more than 8 Mg per hectare per year. This is despite the enormous pressure on South African wastewater treatment plants to dispose of or utilise their sludge in an environmentally sustainable way. This limit has recently been increased to 10 Mg per hectare per year (Snyman and Herselman, 2006). Nevertheless, the problem of sludge disposal still persists.

Generally, sludge of acceptable quality for agricultural use is applied according to crop nitrogen requirements (Milne and Graveland, 1972; Dotson, 1973), but some studies have shown that this approach may lead to a build-up of phosphorus in the soil profile (Pierzynski, 1994; Maguire et al., 2000, Tesfamariam et al., 2009). While these sludge application limits may be appropriate for most agronomic crops, can they be exceeded for perennial dryland pasture without compromising the environment? Perennial grasses have the potential to reduce nitrate leaching compared to annual crops due to their established root system. They are considered a good choice for repeated sludge applications because of their efficient nitrogen utilisation under intensive management practices and because a number of harvests can be made in a year (Bary et al., 2001). If sludge application rate can be increased for dryland pasture without compromising the environment, this management option may prove a better disposal method and help reduce the huge amounts of sludge that are usually left unutilised.

This study investigates the effect, on pasture yield and soil nitrate and phosphorus levels, of applying sludge at a rate higher than the recommended limits. It is hypothesised that municipal sludge loading above the recommended limit would improve weeping lovegrass hay yield without causing excessive nitrate leaching. It is also hypothesised that surface application of FeCl₃ treated municipal sludge (<1 P:Fe molar ratio) according to weeping lovegrass N demand would result in the accumulation of total and Bray-1P in the soil profile.

MATERIALS AND METHODS

Field site description

Field experiments were conducted at the East Rand Water Care Works (ERWAT), Johannesburg, Gauteng, South Africa. The study site is situated at an elevation of 1 577 m above sea level, latitude 26° 01' 01" S and longitude of 28° 16' 55" E. The total annual rainfall of the area ranged between 405 mm in 2006/07 and 710 mm in 2007/08, mainly during the months of October to March. The soil of the experimental site is a clay loam, Hutton soil form (Soil Classification Working Group, 1991) having an average clay content of 38%, and pH (H_2O) of 5.73. At the onset of the study, the mean cation exchange capacity of the soil (ammonium acetate extract) was 11 cmol·kg⁻¹ and the electrical conductivity ranged from 8 mS·m⁻¹ at 1.2 m depth to 36 mS·m⁻¹ in the top 0.3 m soil layer.

Sludge characteristics

The sludge used in this study was anaerobically digested and paddy-dried, collected from Vlakplaas Wastewater Treatment Plant. According to the current South African sludge guideline (Snyman and Herselman, 2006), this sludge is classified as pollutant Class 'a' due to its low heavy metal content. Based on low levels of faecal coliform and helminth ova, the sludge is classified as microbiological Class 'A'. With respect to sludge stability, the sludge is classified as Class '1' due to its low odour and low vector attraction characteristics. The current South African guideline for the utilisation and disposal of wastewater sludge (Snyman and Herselman, 2006) allows such quality sludges to be utilised in agriculture without restriction, as long as the N applied does not exceed crop demand, with the upper limit set at 10 Mg ha⁻¹·yr⁻¹. Selected properties of this A1a sludge are presented in Table 1.

Field trial plots and treatments

Plots of 25 m^2 were arranged in a randomised complete block design comprising 4 replications of 4 treatments. The trial was laid out to accommodate widely different levels of bio-solid application.

		TABLE	1				
Some prop	Some properties of sludge used during the 2004/05 –						
	2007/08 growing seasons						
Parameter measured	Unit	2004/05	Ye	ar	2007/08		
N	0/	2004/05	1 00 /	2000/07	2007/08		
IN NUL N	70	2.012	1.004	4.064	7.660		
NH ₄ N	mg·kg ·	2 018	4 362	4 064	/ 660		
NO ₃ _N	mg∙kg⁻¹	183	6	40	11		
Р	%	1.962	1.844	2.76	2.24		
P – Bray1	mg∙kg ⁻¹	166	154	40	66		
Total C	%	23	20	21	20		
Water content	%	46	30	28	38		
EC	mS⋅m ⁻¹	1 814	1212	1 412	3 110		
К	mg∙kg⁻¹	3 804	710	689	1 356		
Ca	mg∙kg⁻¹	25 116	13 062	17 450	10 042		
Mg	mg∙kg⁻¹	5 358	591	829	1145		
pH (H ₂ O)		6.01	6.2	6.02	6.08		
Cd	mg∙kg⁻¹	1.63	0.07	0.15	18.91		
Hg	mg∙kg⁻¹	1.70	0.02	0.03	1.81		
Cr	mg∙kg⁻¹	51.93	1.50	2.92	503.8		
As	mg⋅kg ⁻¹	7.08	0.18	0.23	17.94		
Pb	mg∙kg ⁻¹	54.46	9.41	1.37	102.0		
Zn	mg·kg ⁻¹	459.9	4.33	20.85	2325		
Ni	mg·kg⁻¹	23.81	1.37	0.97	144.5		
Cu	mg·kg⁻¹	97.2	3.21	4.59	526.8		

Treatments consisted of 3 sludge rates (4, 8, and 16 Mg ha⁻¹·yr⁻¹) and an unamended zero control. The annual sludge application rate was split into two so that half was applied at the beginning of the season and the remaining half following the first cut.

At the onset of the study, during the 2004/05 growing season, sludge was broadcast over the soil surface and immediately incorporated into the top 10 cm soil layer with a manually-operated, diesel-powered rotovator (Agria). After sludge incorporation, the soil was levelled using rakes. A mixture of weeping lovegrass (*Eragrostis curvula*) (10 kg·ha⁻¹) and teff (*Eragrostis teff*) (6 kg·ha⁻¹) was planted on 15 November 2004 and a hand-drawn roller was used to ensure good seed-soil contact for better germination. During the rest of the study period, however, sludge was broadcast over the soil surface of the already established weeping lovegrass plots and left on the soil surface without incorporation. Sludge application and haycutting dates are presented in Table 2.

Weather data

Weather data were collected from an automatic weather station located about 100 m from the experimental site. The automatic

TABLE 2 Sludge application and hay cutting dates for Weeping lovegrass during the 2004/05 to 2007/08 growing seasons at ERWAT, Ekurhuleni district, South Africa							
Growing	Sludge appl	ication date	Hay cutting date				
season	First	Second	First	Second			
2004/05	14/11/2004	20/02/2005	17/02/2005	22/05/2005			
2005/06	01/11/2005	20/02/2006	31/01/2006	11/05/2006			
2006/07	20/10/2006	10/01/2007	09/01/2007	16/04/2007			
2007/08	26/09/2007	14/01/2008	11/01/2008	16/04/2008			

	TABLE 3																				
	precipitation during the 2004/05 to 2008/09 growing seasons, ERWAT, Ekurhuleni district Pretoria, South Africa																				
Period			20	04		2005				20	06		2007			2008					
		Temp	eratur	e (°C)	Rain	Temp	peratur	e (°C)	Rain	Temp	peratur	re (°C)	Rain	Temp	eratur	e (°C)	Rain	Temp	peratu	re (°C)	Rain
Month	Weeks	Max.	Min.	Ave.	(mm)	Max.	Min.	Ave.	(mm)	Max.	Min.	Ave.	(mm)	Max.	Min.	Ave.	(mm)	Max.	Min.	Ave.	(mm)
Jan.	1–2					29	16	23	111	26	17	21	51	29	13	21	47	24	15	20	59
	3-4					26	16	21	56	26	15	21	57	29	14	21	24	23	14	18	148
Feb.	1–2					29	16	22	17	26	15	20	103	30	13	21	30	25	14	19	56
	3-4					27	15	21	79	27	15	21	70	32	14	23	0	27	15	21	5
Mar.	1–2					27	12	20	27	24	12	18	13	30	13	22	6	24	14	19	117
	3-4					25	12	18	44	23	12	18	38	27	11	19	7	22	11	16	42
Apr.	1–2					23	11	17	45	24	9	17	10	26	10	18	0	24	11	18	17
	3-4					22	8	15	18	21	8	14	9	21	8	15	19	24	10	17	0
May	1–2					23	5	14	1	21	5	13	0	21	5	13	0	22	10	16	33
	3-4					2	4	13	0	19	2	10	3	19	0	10	0	19	8	13	10
June	1–2					22	3	12	0	22	3	12	0	18	3	10	29	17	6	12	14
	3-4					20	2	11	0	18	1	9	0	18	1	9	0	18	6	12	3
July	1–2					19	1	10	0	20	2	11	0	17	0	8	0	16	5	10	0
	3-4					22	2	12	0	22	4	13	0	20	1	11	0	18	6	12	0
Aug.	1–2					22	4	13	0	20	3	11	10	21	2	11	0	20	7	14	0
	3-4					24	7	15	0	21	6	14	30	22	4	13	0	22	9	15	0
Sep.	1–2					26	8	17	0	24	6	15	0	27	13	20	0	25	9	17	0
	3-4					29	10	19	0	26	8	16	0	25	11	18	17	23	9	16	0
Oct.	1–2					28	10	19	0	28	12	20	0	21	10	16	85	26	12	19	0
	3-4					29	12	20	12	31	14	22	13	22	11	16	34	27	14	20	62
Nov.	1–2	30	15	22	12	28	13	20	55	28	13	21	42	25	13	19	4	26	14	20	52
	3-4	30	15	23	29	28	13	21	54	26	14	20	75	26	14	20	45	25	15	20	45
Dec.	1–2	28	16	22	72	26	14	20	35	30	15	22	13	23	13	18	68	27	15	21	59
	3-4	28	15	22	64	28	13	20	68	29	17	23	121	25	14	19	12	27	15	21	67

weather station consisted of an LI 200X pyranometer (LiCor, Lincoln, Nebraska, USA) for measuring solar radiation, an electronic relative humidity and temperature sensor (Thermistor Humitter 50Y) installed in a gill screen (R.M. Young, Minnesota, USA), an electronic cup anemometer to measure wind speed (R.M. Young, Minnesota, USA), an electronic rain gauge Model TR-525M-R2 (Texas Electronic Inc., Dallas, Texas, USA), and a CR10X data-logger (Campbell Scientific Inc., Utah, USA). Two-weekly mean maximum, minimum and average temperature as well as two-weekly cumulative precipitation are presented in Table 3.

Soil solution sampling and analyses

Nitrate leaching was monitored by wetting front detectors (WFDs) installed both at 0.3 and 0.6 m depths located in the middle of a plot. The detectors were installed in the control, 8 and 16 Mg ·ha⁻¹·yr⁻¹ plots. Soil solution samples collected from the wetting front detectors were analysed for nitrate concentration using a C99 Multiparameter Bench Photometer (Hanna Instruments, Italy).

Plant sampling

Above-ground samples for hay yield determination were collected 0.05 m above the soil surface at flowering, from a 1 m^2 area. These were then dried in a forced-air oven at 60°C for

http://dx.doi.org/10.4314/wsa.v39i4.9 Available on website http://www.wrc.org.za ISSN 0378-4738 (Print) = Water SA Vol. 39 No. 4 July 2013 ISSN 1816-7950 (On-line) = Water SA Vol. 39 No. 4 July 2013 48 h to determine above-ground biomass. Above-ground biomass was calculated as the sum of leaf and stem. In addition, a hand grab of grass samples was collected at harvest from each plot for grass N and P uptake determination. A 0.5 m border was left around all sides of each plot during sampling to eliminate border effects.

Soil sampling

At the beginning of the study, before treatment application, and at the end of each growing season, soil samples were collected from each plot, using an auger, from the following layers: 0-0.1 m, 0.1-0.3 m, 0.3-0.5 m, and 0.5-0.8 m. Replicate samples from each layer in the same plot were combined and mixed to make a single homogeneous soil sample. All soil samples were dried and pulverised. The dried and ground soil samples were digested and analysed for N, P, NO₃⁻, NH₄⁺, and Bray-1P.

Plant, sludge and soil chemical analyses

Total P in sludge, soil, and plant samples were determined after wet acid digestion using an Inductively Coupled Plasma Optical Emission Spectrometer (ICP-OES) (SpectroFlame Modula; Spectro, Kleve, Germany). Plant extractable soil P was analysed using the Bray-1 extraction method, following standard procedures (Non-affiliated Soil Analysis Work Committee, 1990). Soil and plant samples were ground to pass through a 150 µm screen and analysed for total C and N using a Carlo Erba NA1500 C/N analyser (Carlo ErbaStrumentazione, Milan, Italy). Soil samples were extracted in 1:5 1 M KCl and tested for ammonium and nitrate with the Lachat Autoanalyzer (Lachat Quick Chem Systems, Milwaukee, WI, USA).

Statistical analyses

Statistical analyses were performed to evaluate the impact of various sludge application rates on hay yield. The statistical analyses were conducted using analysis of variance (ANOVA) and general linear model (GLM) procedures of Windows SAS version 9.0 (SAS Institute, 2002), to determine significant treatment effects on measured response variables. When treatment effects were found to be significant, Fisher's protected LSD at the 0.05 level was used to separate means.

RESULTS AND DISCUSSION

Hay yield

Hay yield increased with increase in sludge rate (Fig 1). A maximum of 17.3 Mg·ha⁻¹ was recorded during the 2007/08 season from the 16 Mg·ha⁻¹ sludge treatment. The increase in yield as a result of sludge addition is attributed to an increased supply of plant nutrients and to improvement of soil physical properties (Ferreiro-Domínguez et al., 2011).

In general, hay yield throughout the study period was much higher than the long-term average values of 6 Mg·ha⁻¹ reported by Dickinson et al. (2004) from Hutton soils receiving similar annual rainfall. This is most probably due to a better nutrient status of the soil from this study compared with the soils reported by Dickinson et al. (2004).

Generally, hay yield was highest in the 2007/08 season and, in addition to a cumulative improvement of soil chemical and physical properties, this higher yield observed during the 2007/08 season may be attributed to the higher rainfall received during the period (Table 3). Miles and Manson (2000) and Dickinson et al. (2004) have reported that weeping lovegrass response to N increases with increase in the availability of water. This may not be unconnected with the increase in the rate of nitrogen mineralisation which increases as soil moisture increases, up to an optimum (Agehara and Warncke, 2005).

Soil total N mass balance

Based on the mass balance calculation of N imported with sludge less N exported with hay, total N from sludge applied according to the initial 8 Mg·ha⁻¹ limit was close to being, but not quite sufficient to satisfy weeping lovegrass N demand (net negative mass balance) (Table 4, Column 4). Negative mass balances of all but the 16 Mg·ha⁻¹ treatment show that the crop utilised N from the soil reserve. Therefore, total N supply from sludge with 2.56% mean N applied according to the initial 8 Mg·ha⁻¹ norm is not sufficient for optimal weeping lovegrass hay production under the prevailing climatic and soil conditions. Doubling of that upper limit sludge norm, however, resulted in a net positive mass balance. This indicates that the total N supply surpassed hay N uptake. The excess N from double the norm was accumulated mainly in the 0–0.1 m soil layer (Fig. 2), because the sludge was surface applied.

Soil profile sampling to a depth of 0.8 m (Table 4, Column 5) showed similar trends to the supply less uptake mass balance



Figure 1 Annual hay yield of weeping lovegrass as affected by 3 sludge application rates, and an unamended control. Letters show significance within growing seasons.



Figure 2



TABLE 4 Cumulative N supply (CUM-NS)), uptake (CUM-NU), and mass balance of a weeping lovegrass treated with three sludge application rates, and an unamended control							
	F	our years o	umulative	mass balar	ice		
Treatment	CUM-NS (kg•ha ⁻¹)	CUM-NU (kg·ha ⁻¹)	CUM-NS less CUM- NU (kg∙ha⁻1)	Change in soil N storage ^a (kg·ha ⁻¹)	Mass balance difference ^ь (kg∙ha⁻¹)		
Control	0	511	-511	-600	89		
4 Mg·ha ⁻¹ ·yr ⁻¹	409	687	-278	-381	103		
8 Mg·ha ⁻¹ ·yr ⁻¹	818	856	-38	-203	165		
16 Mg·ha ⁻¹ ·yr ⁻¹	1 637	988	649	330	319		

^aChange in soil N storage refers to final less initial soil profile N content change to a depth of 80 cm.

^bMass balance difference refers to the difference between (CUM-NS less CUM-NU) and change in soil N storage.

(Table 4, Column 4). According to this profile analysis, the 16 Mg·ha⁻¹ sludge rate resulted in a net positive mass balance while sludge applied at the rate of 8 Mg·ha⁻¹ had a net negative

TABLE 5						
Residual nitrate mass in the top 0.5 m soil stratum of						
weeping lovegrass plots treated with 3 sludge rates, and an						
unamended control treatment						
	1					

Treatment	Initial	After 2 nd hay cut in 2005/06	After 2 nd hay cut in 2007/08
		kg∙ha⁻¹	
Control	96	60	18
4 Mg·ha ⁻¹ ·yr ⁻¹	96	62	18
8 Mg·ha ⁻¹ ·yr ⁻¹	96	52	16
16 Mg·ha ⁻¹ ·yr ⁻¹	96	51	58

mass balance. Interestingly, however, there was a net positive difference between the two mass balances: supply less uptake (CUM_NS less CUM-NU) and change in storage between final and initial soil profile N contents (Change in soil N storage) (Table 4, Column 6). This difference increased with increase in sludge application rate (mass balance difference).

The most probable cause for the mass balance difference was ammonia volatilisation losses, which is not accounted for in the N import less export mass balance. This is because the sludge used in this study was anaerobically digested with about 20-25% of total N in ammonium form. In addition, the sludge was surface applied. Previous studies conducted by Adamsen and Sabey (1987) showed that 40.3% of the NH₄-N from surface-applied sludge could be lost as NH₂ gas during the first two weeks of its application. This was in contrast to 0.35% loss from an incorporated sludge reported in the same study. Martines et al. (2010) reported a 35% loss as ammonia, of the total NH₄-N in a surface-applied sludge. Some other studies have also shown that up to 89% of the initial ammonium could be lost in the form of ammonia gas from a surface-applied anaerobicallydigested sludge (Henry et al., 1999). Other possible sources of the differences include sampling errors, N content variation within the sludge matrix, soil heterogeneity, and probably denitrification (which is not expected to dominate under dryland cropping), and leaching (which could have been insignificant due to the low rainfall).

Residual nitrate and nitrate leaching

Residual nitrate in the top 0.5 m soil layer of all treatments, including sludge applied at 16 Mg·ha⁻¹, remained less than the initial amount throughout the study period (Table 5). The reduction in nitrate content of all treatments was evident in the 0–0.3 m soil stratum, while the content in the 0.3–0.8 m layer remained similar to initial values (Fig. 3). It was also evident that sludge applied at 16 Mg·ha⁻¹ had relatively lower residual nitrate than that of lower sludge rates in 2005/06, but this was higher at the end of the 2007/08 growing season.

Although residual nitrate at the end of the study was relatively higher for the 16 Mg·ha⁻¹·yr⁻¹ sludge treatment than other treatments, it was still low and was almost half of the initial mass. The main reason for monitoring residual nitrate after harvest was that nitrate leaching under dryland conditions usually takes place at the beginning of the rainy season, especially before active root nutrient uptake in the presence of high rainfall and residual soil nitrate. Nitrate is susceptible to diffusion and transport through mass flow with soil water, because there is little tendency for the mostly negatively-charged soil colloids to adsorb the negatively-charged nitrate (Cameron and Haynes, 1986).

In this specific study the mean annual rainfall was low (405 mm in 2007) to moderate (710 mm in 2008). The wetting



Residual nitrate before treatment application (initial) and after 4 consecutive years of sludge application at 3 rates (4, 8, and 16 Mg·ha⁻¹) and a zero control

TABLE 6 Residual ammonium mass in the top 0.5 m soil stratum after every second weeping lovegrass hay cut during the 2004/05 to 2007/08 growing seasons							
Treatment	reatment Initial After 2 nd hay After 2 nd (kg·ha ⁻¹) cut in 2005/06 cut in 20 (kg·ha ⁻¹) (kg·ha ⁻¹)						
Control	65	16	20				
4 Mg·ha ⁻ ·yr ⁻¹	65	41	38				
8 Mg·ha ⁻¹ ·yr ⁻¹	g·ha ⁻¹ ·yr ⁻¹ 65 31 46						
16 Mg·ha ⁻¹ ·yr ⁻¹	65	36	65				

front detectors buried at 0.3 m depth responded only 4 times during the 4-year study period. The dates of response and the corresponding nitrate concentrations from the 16 Mg·ha⁻¹·yr⁻¹ sludge treatment were: 21/02/2005 (10 mg· ℓ^{-1} NO₃), 01/03/2006 (14 mg· ℓ^{-1} NO₃), 22/01/2008 (8 mg· ℓ^{-1} NO₃), and 16/03/2008 (11 mg· ℓ^{-1} NO₃). The control and 8 Mg·ha⁻¹· yr⁻¹ sludge treatments had similar or lower nitrate concentrations during the same time period. None of the WFDs buried at 0.6 m, however, responded. Therefore, considering the low to moderate rainfall experienced during the study period, low residual nitrate, and low nitrate concentrations collected during very few events might indicate that nitrate leaching was minimal during the study period.

Residual ammonium

Residual ammonium in the top 0.5 m soil stratum remained equal or less than initial values for all treatments (Table 6). Residual ammonium, however, increased with increase in sludge application rate at the end of the 2007/08 growing season, but did not show any specific trend in 2005/06.

Despite the net positive total N mass balance of the 16 Mg·ha⁻¹·yr⁻¹ sludge treatment (Table 4, Columns 4 and 5), residual ammonium and nitrate remained similar to or less than initial values. This indicates that a large fraction of the N in the soil is present in organic form. This might also indicate that the ammonium added from the sludge was either nitrified or taken up by the plants. The possibility for ammonium to leach below the active root zone (0–0.6 m) in this specific soil type under the prevailing rainfall and sludge rates is unlikely, considering that primarily, the predominantly negatively charged soil clay

TABLE 7 Cumulative total P supply (CUM-PS), uptake (CUM-PU), and mass balance of a weeping lovegrass treated with 3 sludge application rates, and an unamended control							
Treatment	Treatment Four years cumulative total P mass balance						
	CUM-PS (kg∙ha⁻¹)	CUM-PU (kg∙ha⁻¹)	CUM-PS less CUM-PU (kg∙ha ⁻¹)	Change in soil P storage (kg·ha ⁻¹)	Mass balance difference (kg·ha ⁻¹)		
Control	0	59	-59	-50	-9		
4 Mg·ha ⁻¹ ·yr ⁻¹	352	73	279	302	-23		
8 Mg·ha ⁻¹ ·yr ⁻¹	705	93	612	660	-48		
16 Mg·ha ⁻¹ ·yr ⁻¹	1 409	102	1 307	1 316	-9		

and organic matter particles can fix ammonium through the process of cation exchange. Moreover, ammonium can easily be immobilised by microbial biomass, and is also readily nitrified (Cameron and Haynes, 1986).

Total P mass balance

Sludge applications rates of 4 Mg·ha⁻¹ and higher resulted in a net positive total P mass balance (CUM-PS less CUM-PU) following 4 years of sludge applications and hay harvest events (Table 7, Column 4). Based on the mass balance calculation of total P imported with sludge less exported with weeping lovegrass hay yield, sludge applications of 4 Mg·ha⁻¹·yr⁻¹ supplied a cumulative excess of 279 kg P ha⁻¹ during the 4-year study.

There was a mass balance difference (Table 7, Column 6) between the P supply less uptake mass balance (Table 7, Column 4) and the final less initial soil profile total P mass balance (Table 7, Column 5). The possible sources of difference are P content variation within the sludge matrix, soil heterogeneity and sampling errors.

The main reason for the accumulation of P in the soil profile was the low sludge N:P ratio compared with that of crops. Therefore, P accumulation is inevitable if sludge is applied according to crop N demand (Shober and Sims, 2003).

Changes in soil P storage from depths of 0.8 m (Table 7, Column 5) also supported the trends for the total P supply less uptake mass balance (Table 7, Column 4). Most of the excess P added with the sludge was located in the 0–0.1 m soil layer with a slight increase in the deeper 0.1–0.3 m soil layer (Fig. 4). The slight total P increment in this soil layer was most probably due to the physical migration of colloidal sludge particles between cracks formed during dry periods of the year, or from preferential flow of particulate P (Jensen et al., 2000; Brock et al., 2007). The grave concern with P surface accumulation is the potential threat to surface water bodies through transport by runoff,



Figure 4

Initial soil profile total P and after 4 consecutive years of municipal sludge application at 3 rates (0, 4, and 8 Mg ha⁻¹ per year) and a zero control in a clay loam soil planted to weeping lovegrass

enhancing the rate of eutrophication in freshwater bodies (Carpenter et al., 1998).

Soil profile residual Bray-1 extractable P

Bray-1P decreased as the sludge application rate increased to 8 Mg·ha⁻¹·yr⁻¹, but increased at higher rates (Table 8). Four years of sludge application according to the initial 8 Mg·ha⁻¹ limit reduced residual Bray-1P by 42%. This is in contrast to the net positive total P mass balance reported for the same treatment in Table 7 Columns 4 and 5. On the other hand, sludge applied at 16 Mg·ha⁻¹ increased residual Bray-1P in the top 0.5 m by 33% and 58%, compared with the control and 8 Mg·ha⁻¹ sludge treatments, respectively.

Generally the mean background Bray-1P concentration of the soil in the 0–0.3 m soil stratum (65 mg·kg⁻¹) was higher than the optimum concentration required for most crops (25–30 mg·kg⁻¹). It was also higher than the concentration for an optimum soil quality (50 mg·kg⁻¹), above which the risk for surface water body pollution increases, as reported by Sims and Pierzynski (2000).

The decline in Bray-1P reported for the 4 and 8 Mg·ha⁻¹ sludge treatments was mainly due to the FeCl₃ added to the sludge at the waste treatment plants, which reduced the solubility of P (O'Connor et al., 2004; Huang et al., 2007). The build-up of Bray-1P reported from doubling of the sludge upper limit (16 Mg·ha⁻¹) is most probably because the P supply from the sludge exceeded the buffer capacity of the soil and sludge (Elliott and O'Connor, 2007), or because of a decline in the sludge's P-sorbing capacity over time (Lu and O'Connor, 2001). It is also possible that the Fe-P minerals may have released P by dissolution, as reported by Huang et al. (2007).

TABLE 8 Residual Bray-1P in the top 0.5 m soil stratum after the second hay cut of dryland pasture (weeping lovegrass) during the 2004/05 to 2007/08 growing seasons								
Treatment	Initial After 2 nd hay cut in After 2 nd hay cut in (kg·ha ⁻¹) 2005/06 2007/08 (kg·ha ⁻¹) (kg·ha ⁻¹) (kg·ha ⁻¹)							
Control	274	282	254					
4 Mg·ha ⁻¹ ·yr ⁻¹	274	253	230					
8 Mg·ha ⁻¹ ·yr ⁻¹	274	150	159					
16 Mg·ha ⁻¹ ·yr ⁻¹	274	367	378					

Therefore, it is apparent from this study that although sludge treated with FeCl₃ reduced P plant availability, it is likely that P availability could also increase at higher rates over time.

Despite the high background concentration and additional P added with the sludge, there were no visible phosphorus toxicity symptoms during the study period. This is most probably due to the high Zn added with the sludge, because previous studies conducted by Loneragan et al. (1979), Safaya (1976), Parker (1997), and Silber et al. (2002) have shown that plant P toxicity is enhanced under Zn-deficient conditions.

CONCLUSIONS

Weeping lovegrass hay yield increased with increase in sludge rate. Highest yield was harvested from years which experienced high rainfall. Sludge applied according to the WRC initial limit of 8 Mg·ha⁻¹·yr⁻¹ was not sufficient to satisfy weeping lovegrass N demand. Doubling that limit did not cause the accumulation of nitrate and ammonium in the soil profile. However, it increased both total and Bray-1P with time. Therefore, both of the initial hypotheses are accepted. It is recommended that long-term model simulations should be conducted under varying conditions in order to get a site-specific real-time ideal sludge application rate.

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